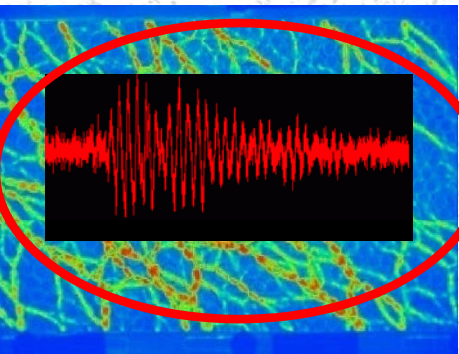


# Weakly vibrated granular packing

*Eric CLEMENT*

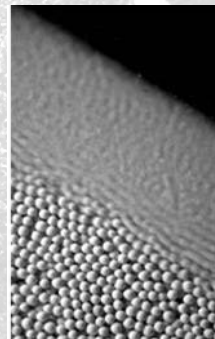
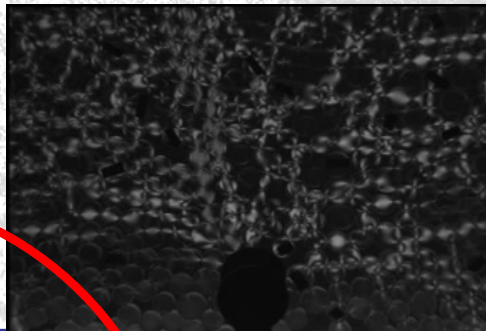


ESPCI-CNRS - Univ.Paris 6 & 7

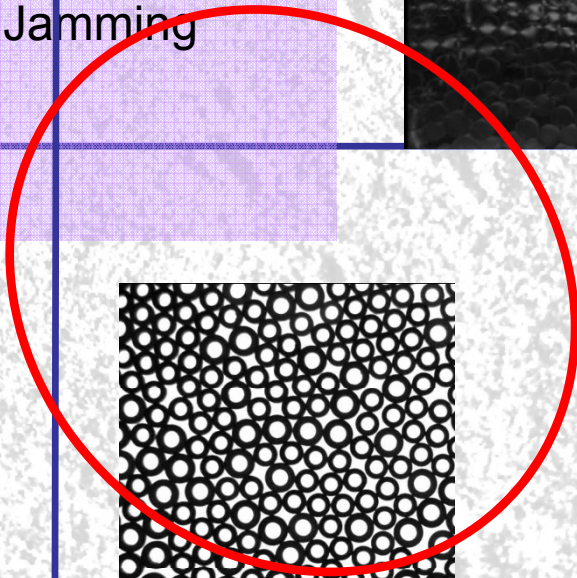


Elastic « fragile » solid

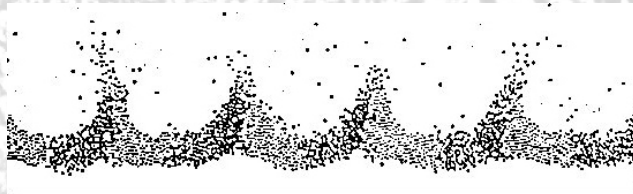
Jamming



shear



Vibrations



# I Introduction

## II Acoustics in granular matter

- NL elasticity
- Mean field failure
- Rigidity transition

## III Surface waves acoustics

- Model
- Surface wave experiments

## IV Acoustic activation

- Intruder thread rheology
- Simple model
- Intruder bead mobility

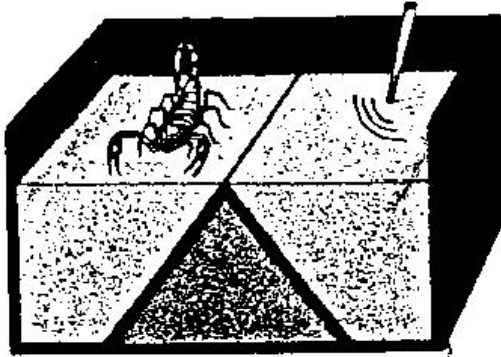
## V Friction activated rheology

- Droplet spreading
- Inertia tribometer

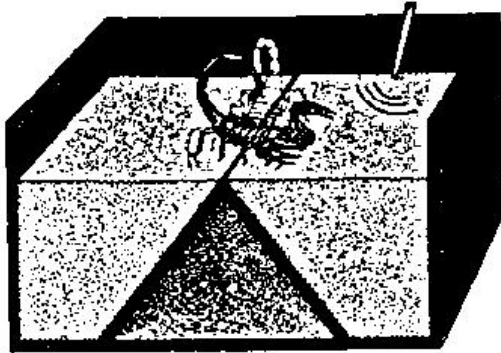
# Scorpion attack

Ph. Brownell, Science **197** 479 (1977)



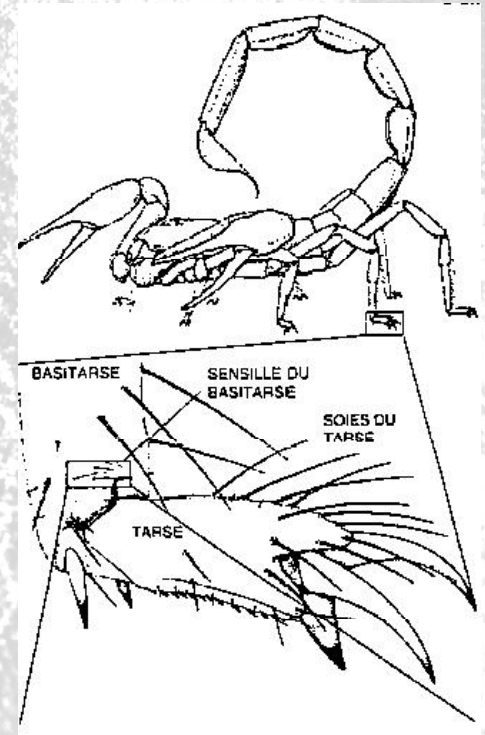


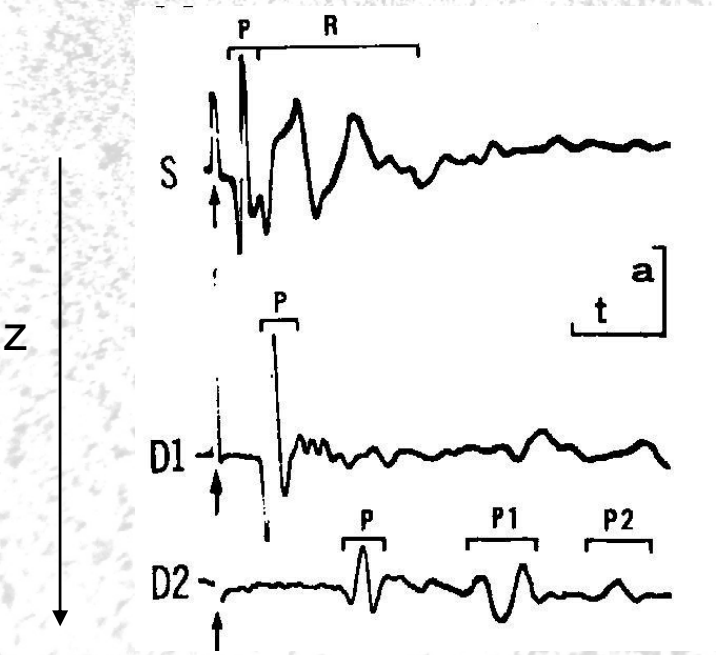
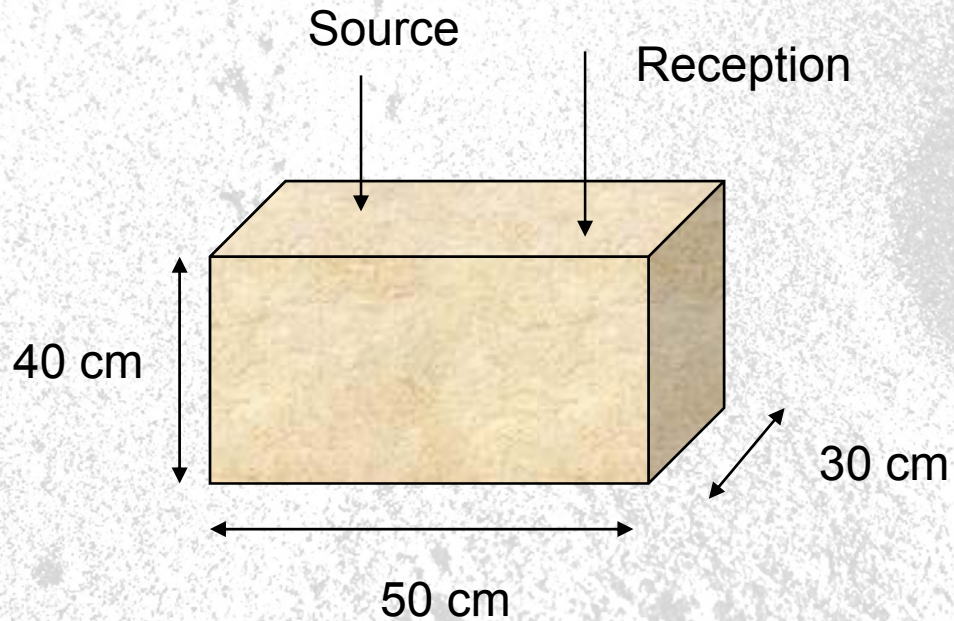
*Paruroctonus mesaensis* use sand surface wave to orient and strike their prey



Slit sensilla detectors

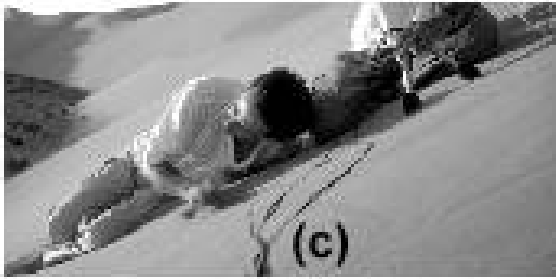
Sensitivity :  $10^{-10}$  m !!





Slow « R » waves : 40-50 m/s

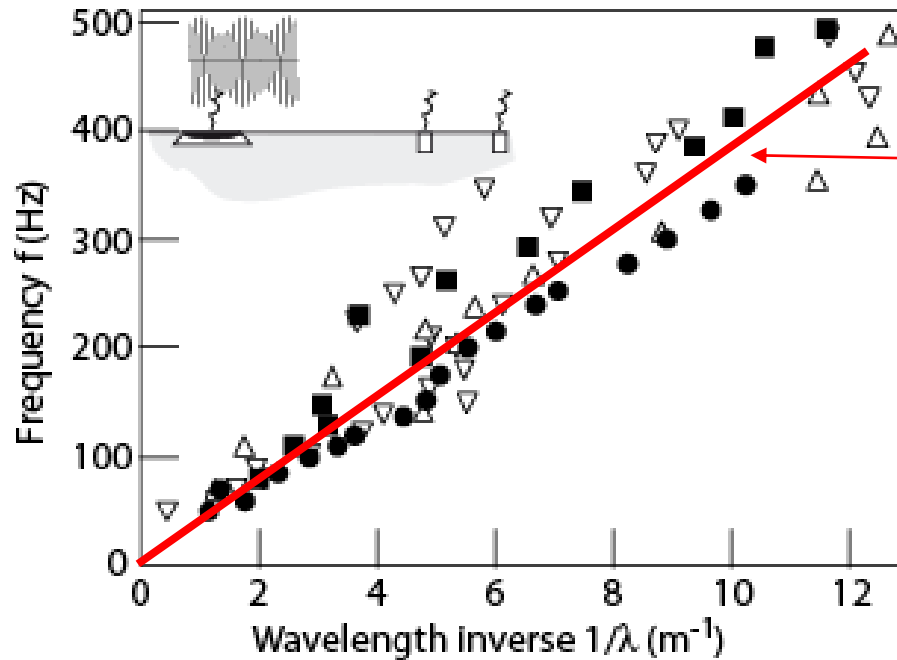
Fast « P » waves : 90-120 m/s



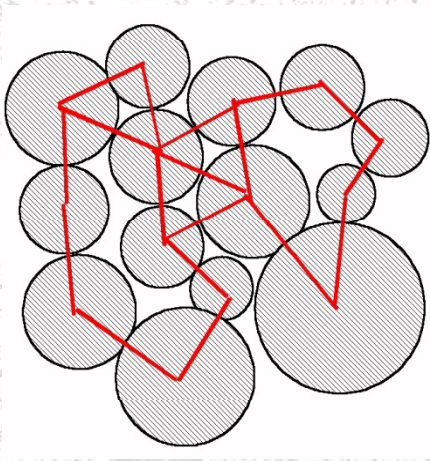
# Field measurements

B. Andreotti, Phys. Rev. Lett. **93**, 238001 (2004)

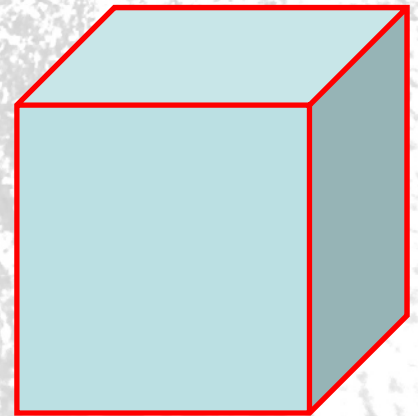
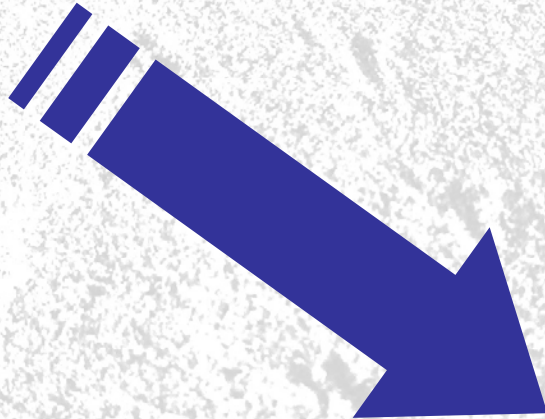
## Dispersion relation



$$c \cong 40 \text{ m / s}$$



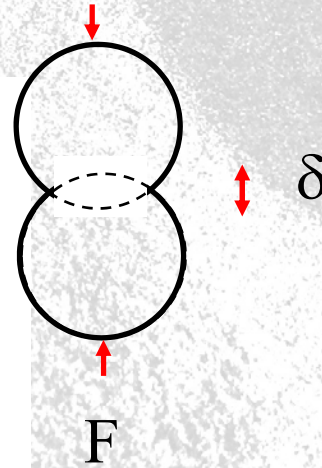
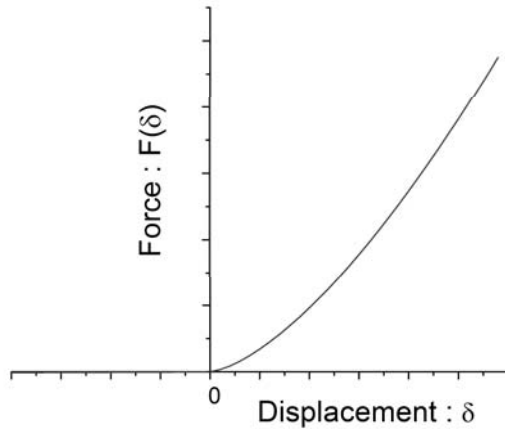
?





# Non linear contact law

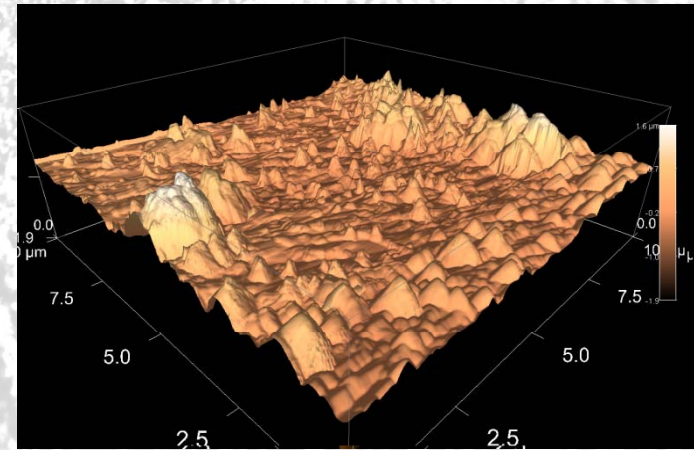
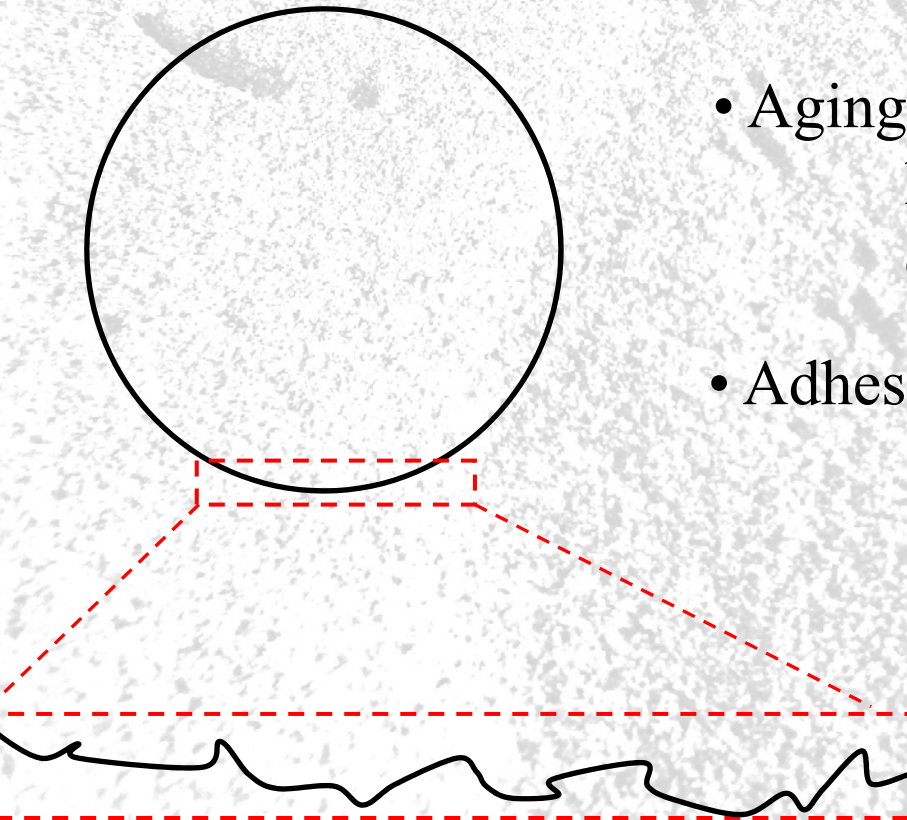
- Hertz contact laws



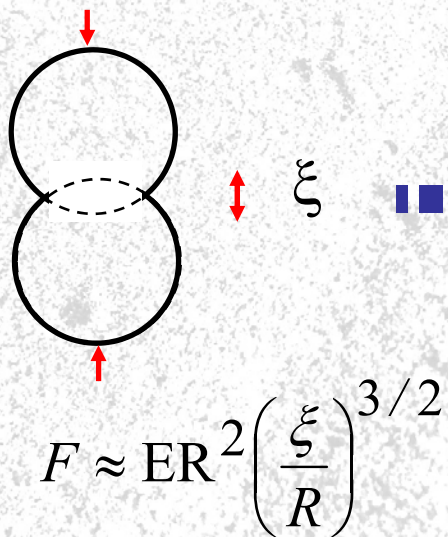
$$F \approx E d^2 \left( \frac{\delta}{d} \right)^{3/2}$$

# Roughness scale

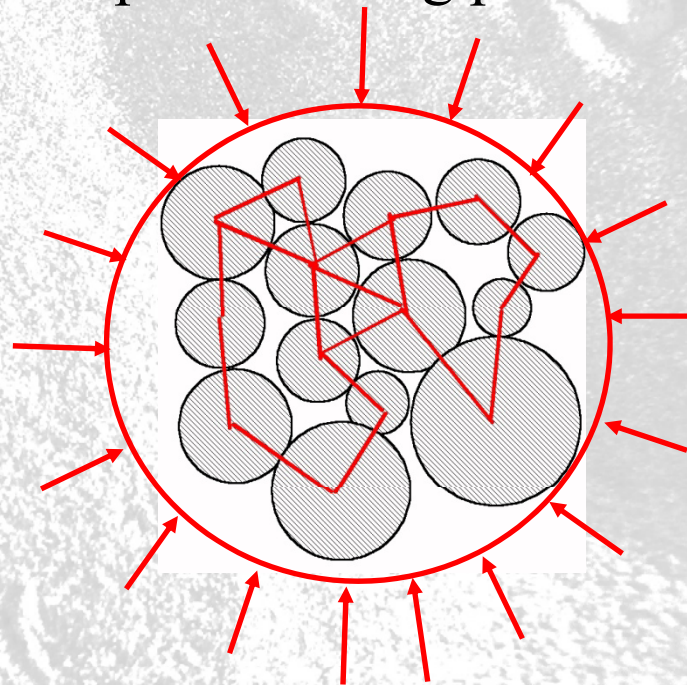
- Solid friction
- Aging  
  humidity  
  contact plasticity
- Adhesion



## Hertz contact law model



$P_0$ : isotropic confining pressure



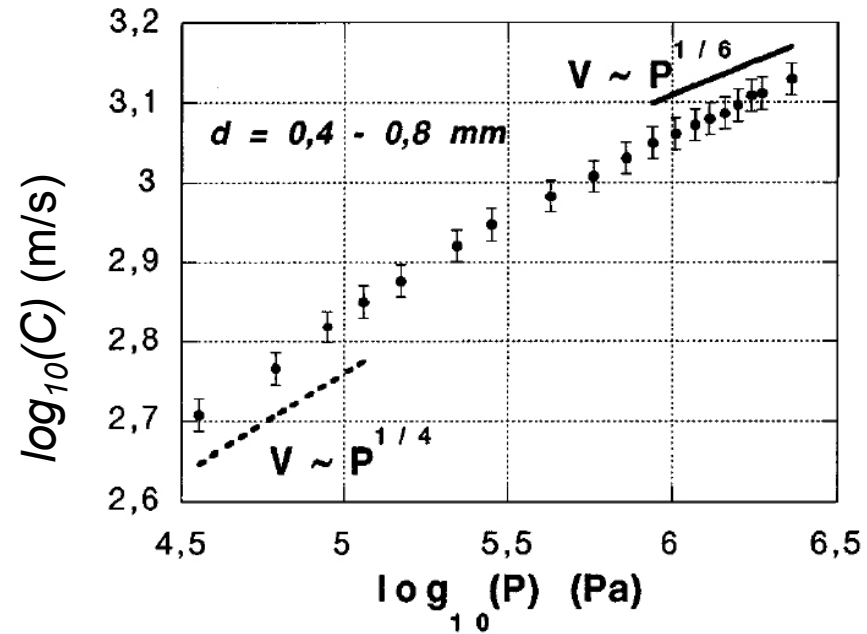
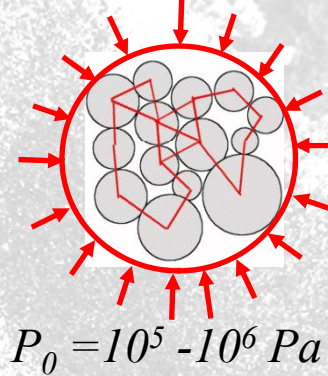
## Macroscopic packing stiffness

$$E_{\text{eff}} \approx E (\phi Z)^{2/3} \left( \frac{P_0}{E} \right)^{1/3}$$

$\phi$ : packing fraction

$Z$ : average number of contact/grains

# Confined packing



Hertz model predicts:

$$C \approx C_0 (\phi Z)^{1/3} \left( \frac{P_0}{E} \right)^{1/6}$$

Jia et al. PRL **82**, 1886 (1999)

A large  $P_0$  evolution of the contact network with confining pressure

$Z \uparrow$  when  $P_0 \uparrow$

But not only !

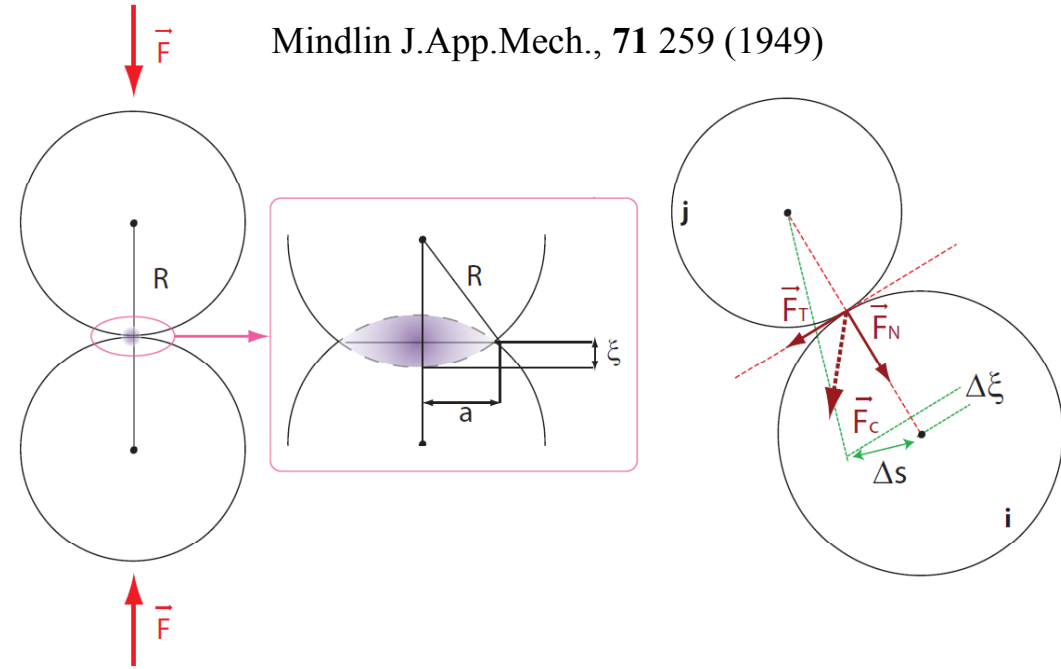
Goddard, Proc.Royal Soc **430** 105 (1990)

de Gennes Europhys. Lett., **35** 145 (1996)

Velický & Caroli Phys. Rev. E **65**, 021307 (2002)

# Contact model

Mindlin J.App.Mech., 71 259 (1949)



$$F_n = \frac{8}{3} \frac{G_g}{1 - \nu_g} R \left( \frac{\xi}{R} \right)^{3/2}$$

Normal contact force

$$\Delta F_t = \frac{8}{2 - \nu_g} G_g R \left( \frac{\xi}{R} \right)^{1/2} \Delta s$$

Tangential contact force

$$\mu_g = \left| \frac{F_t}{F_n} \right|$$

Coulomb yield criterion

# Mean field calculation

Walton J. Mech. and Phys. Sol. **35** 213 (1987)  
Johnson & Norris J. Appl. Mech. **64** 39 (1997)

Bulk modulus

$$K_{\text{MF}} = \frac{1}{3\pi(1-\nu_g)} \frac{G_g}{(\Phi z)^{2/3}} \left( \frac{3\pi(1-\nu_g)}{2G_g} P \right)^{1/3}$$

Shear modulus

$$G_{\text{MF}} = \left( \frac{1}{1-\nu_g} + \alpha \frac{3}{2-\nu_g} \right) \frac{G_g}{5\pi} (\Phi z)^{2/3} \left( \frac{3\pi(1-\nu_g)}{2G_g} P \right)^{1/3}$$

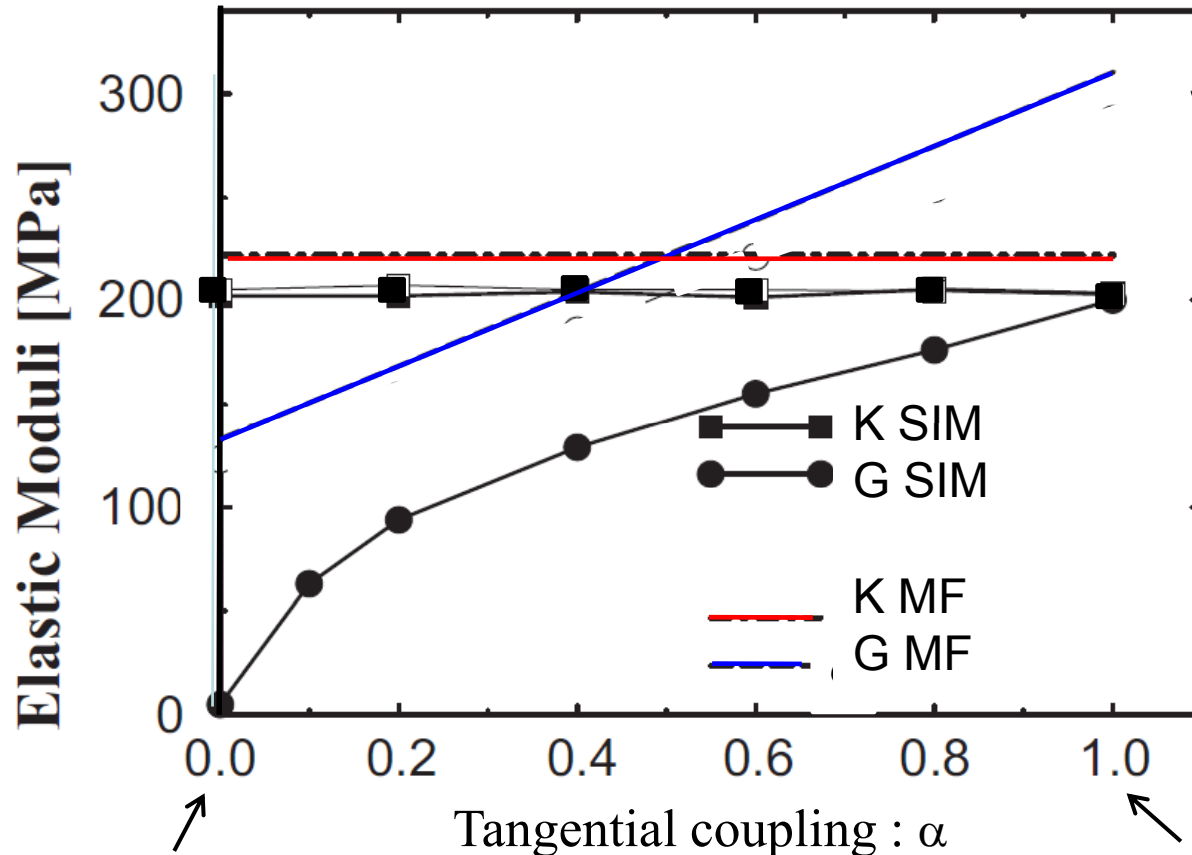
$\alpha=0$  no friction

$\alpha=1$  infinite friction

# Mean field failure

Numerical simulations

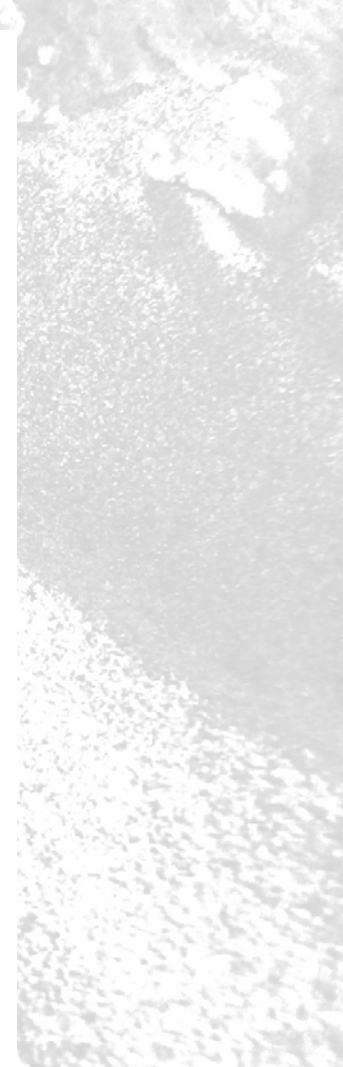
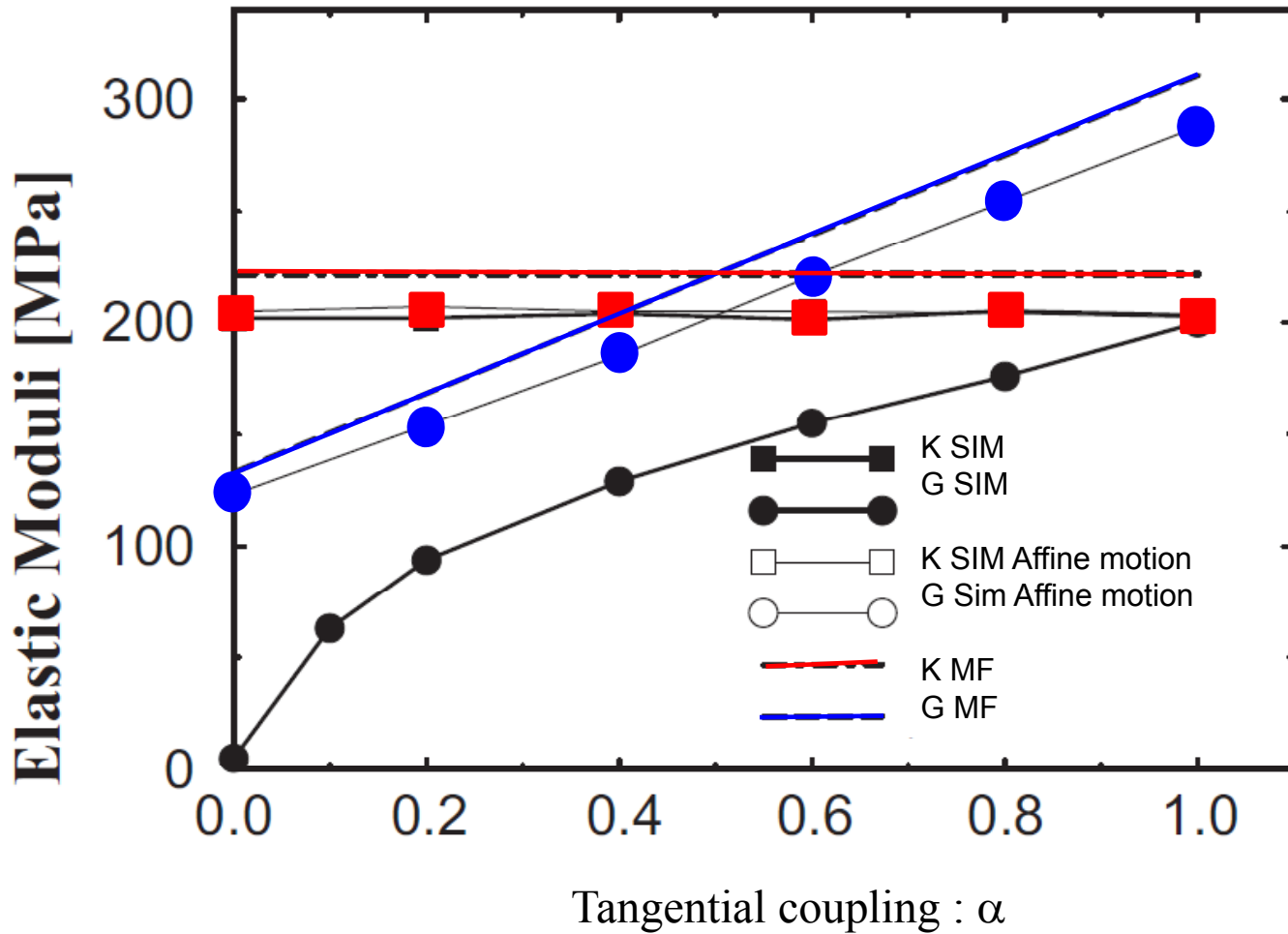
H.A. Makse et al. Phys. Rev. Lett. **83**, 5070 (1999)  
Phys. Rev. E **70**, 061302 (2004)



$\alpha=0$  no friction

$\alpha=1$  infinite friction

Major failure of shear modulus  $G$



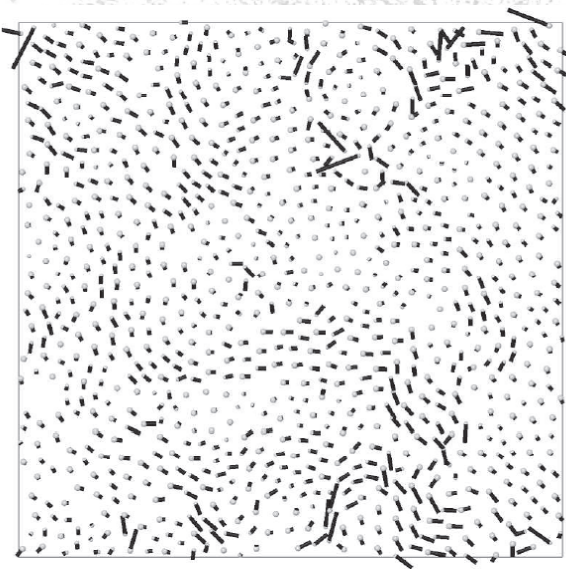
- Affine motion hypothesis breaks down at the granular level
- Granular packing reorganizes



# Elastic anomalies at the rigidity transition

Isostatic critical point ( $\alpha = 0$ )

$$\mu = 0 \quad Z_c = 2d$$

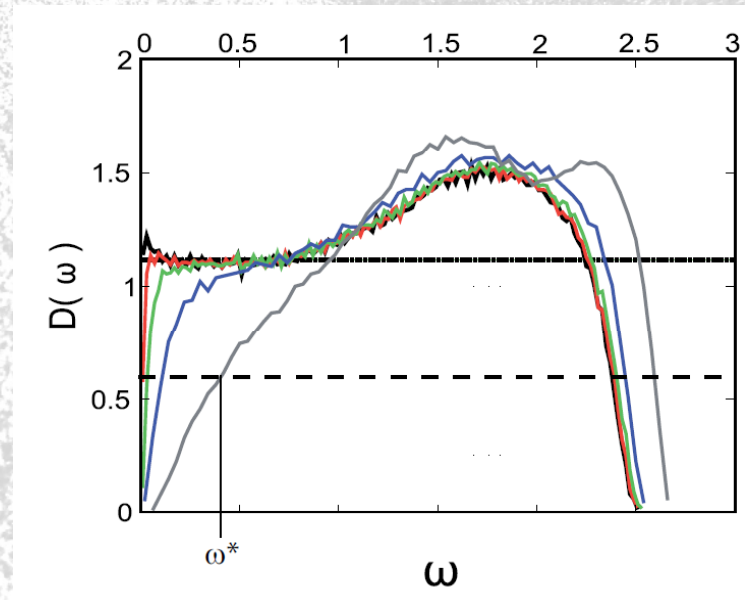


No affine collective motion

O'Hern et al. Phys. Rev. E **68**, 011306 (2003)

Wyart et al., Phys. Rev. E **72**, 051306 (2005)

Agnolin & Roux Phys. Rev. E **76**, :061304(2007)



Soft-modes anomalies

$$\begin{aligned} Z - Z_c &\sim (\phi - \phi_c)^{1/2} \\ P &\sim (\phi - \phi_c)^{3/2} \end{aligned}$$



$$\frac{G}{K} \propto P^{1/3}$$

# Surface wave acoustics of granular packing under gravity

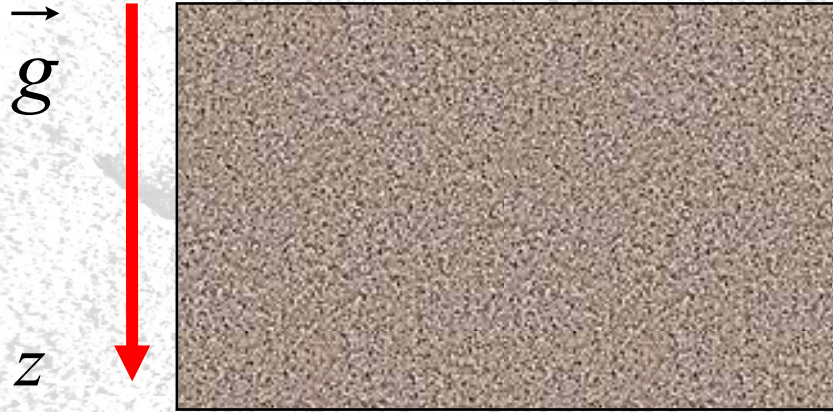
*With L ena ic BONNEAU and Bruno ANDREOTTI*  
*PMMH*  
*ESPCI-CNRS-PARIS 6- PARIS 7*

Refs

Bonneau et al. PRE **75** 016602 (2007)

Bonneau et al. PRL **101**, 118001 (2008)

# Surface wave propagation



Under gravity

$$P = \rho g z$$

$$C \approx C_0 (\phi Z)^{1/3} \left( \frac{P}{E} \right)^{1/6}$$

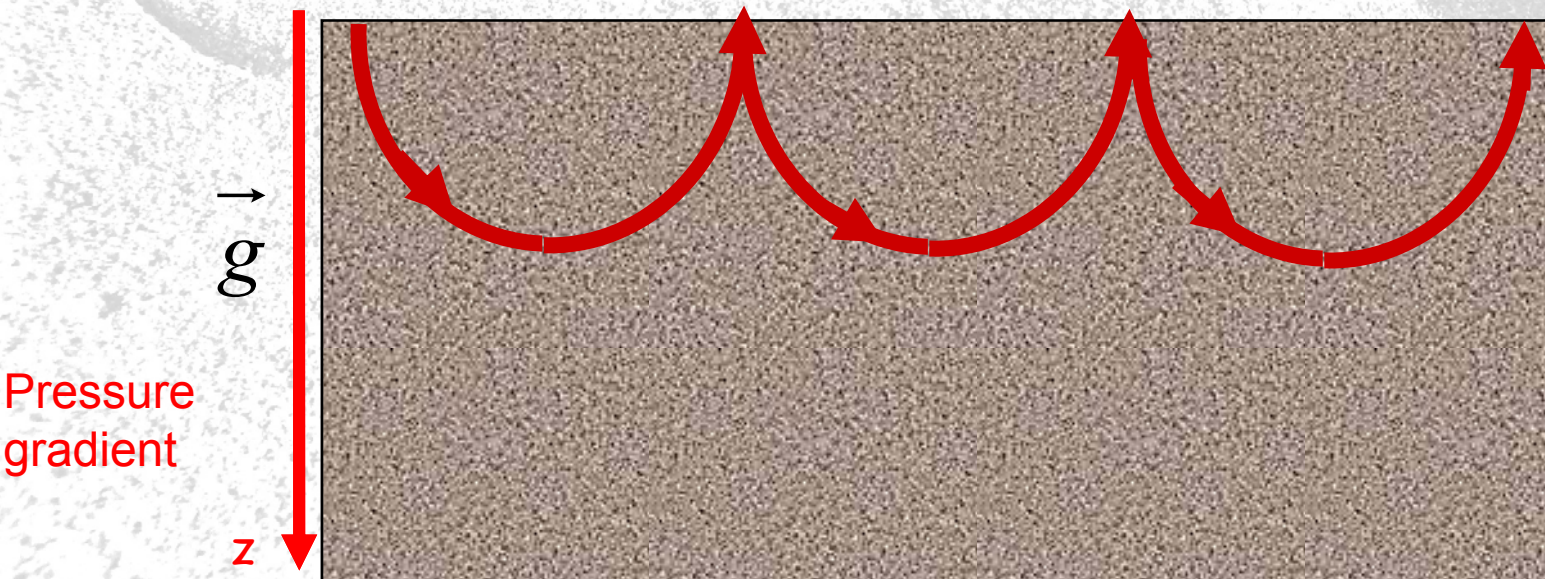
$\Rightarrow$

$$C \propto Z^{1/6}$$

# A mirage effect

$$c \propto z^{1/6}$$

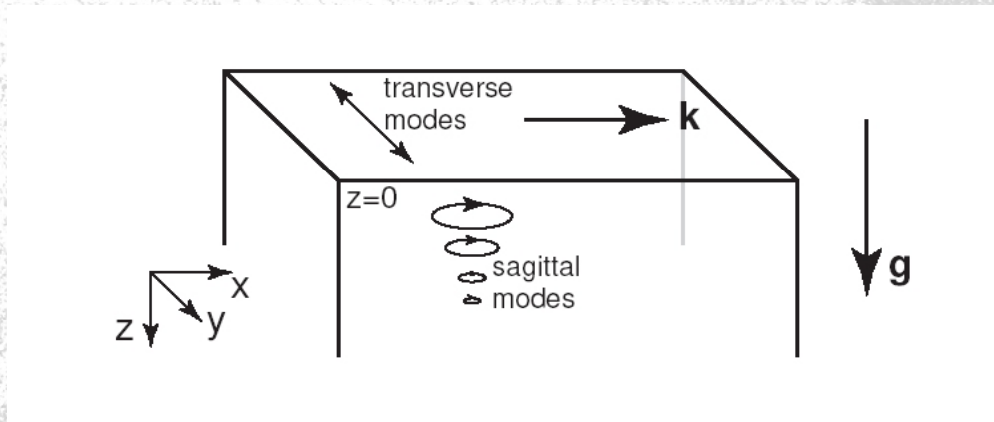
The wave is refracted toward the surface



- No bulk wave propagation !
- Sand packing behave as a index gradient waveguide

# A theoretical calculation

Bonneau et al. PRE 75 016602 (2007)



$$F_{el} = E\delta^{1/2} \left( \frac{2}{5} \mathcal{B} u_{ll} \delta^2 + \mathcal{A} u_s^2 \right)$$

Elastic free energy

Jiang and Liu PRL 91,144301 (2003)

$$\delta = -Tr(u_{ij})$$

Volumic compression

$$u_s^2 = u_{ij}^0 u_{ij}^0$$

Shearing strain

E : Material Young's modulus

$\mathcal{B}$  and  $\mathcal{A}$  dimensionless constants

# Stress/strain relation

$$\sigma_{ij} = E\sqrt{\delta} \left( B\delta\delta_{ij} - 2Au_{ij}^0 + \frac{Au_s^2\delta_{ij}}{2\delta} \right)$$

Boussinesq (1873)

new

- $B$  coupling with bulk compression
- $A$  coupling with shear strain

# Mean-field values of the model parameters

$$E = \frac{8 G_g}{3(1-\nu_g)}$$

$G_g$  grain's shear modulus  
 $\nu_g$  grain's Poisson ratio  
 $E$  grain's Young's modulus

$$A_{MF} = \frac{z\Phi}{3^{3/2}5\pi(1+\nu_g)} \left( \frac{1}{1-\nu_g} + \frac{3\alpha}{2-\nu_g} \right)$$

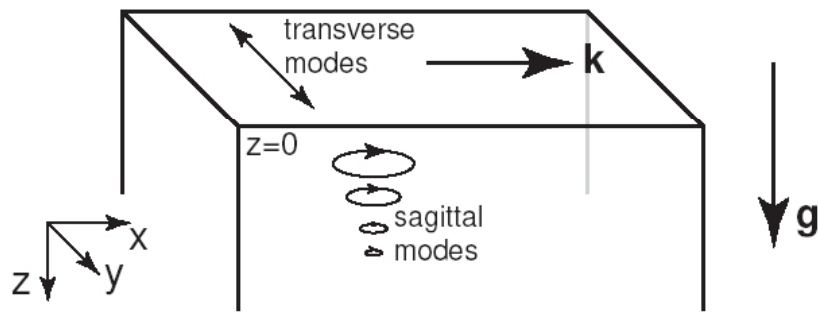
Frictionless grains  $\alpha=0$

Infinite friction grains  $\alpha=1$

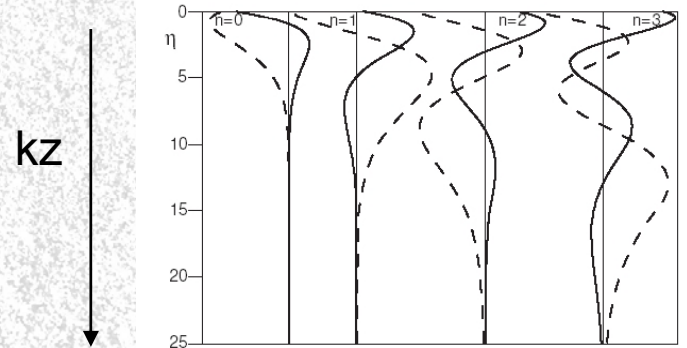
$$B_{MF} = \frac{5}{3} A_{MF}$$

$$B_{MF} = \frac{5}{7} A_{MF}$$

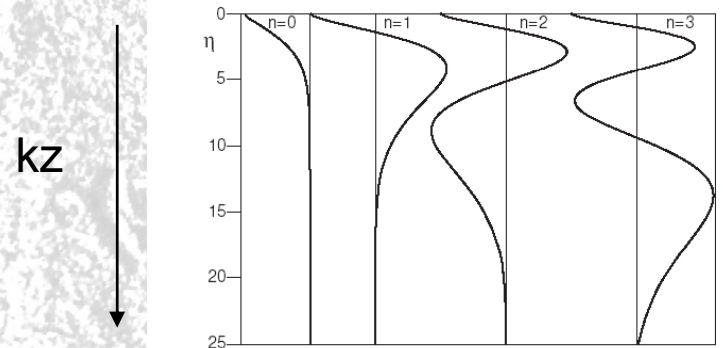
# Surface modes



## Sagittal modes



## Transverses modes



- Modes localized in depth

$$l_p \propto n\lambda$$

Penetration length



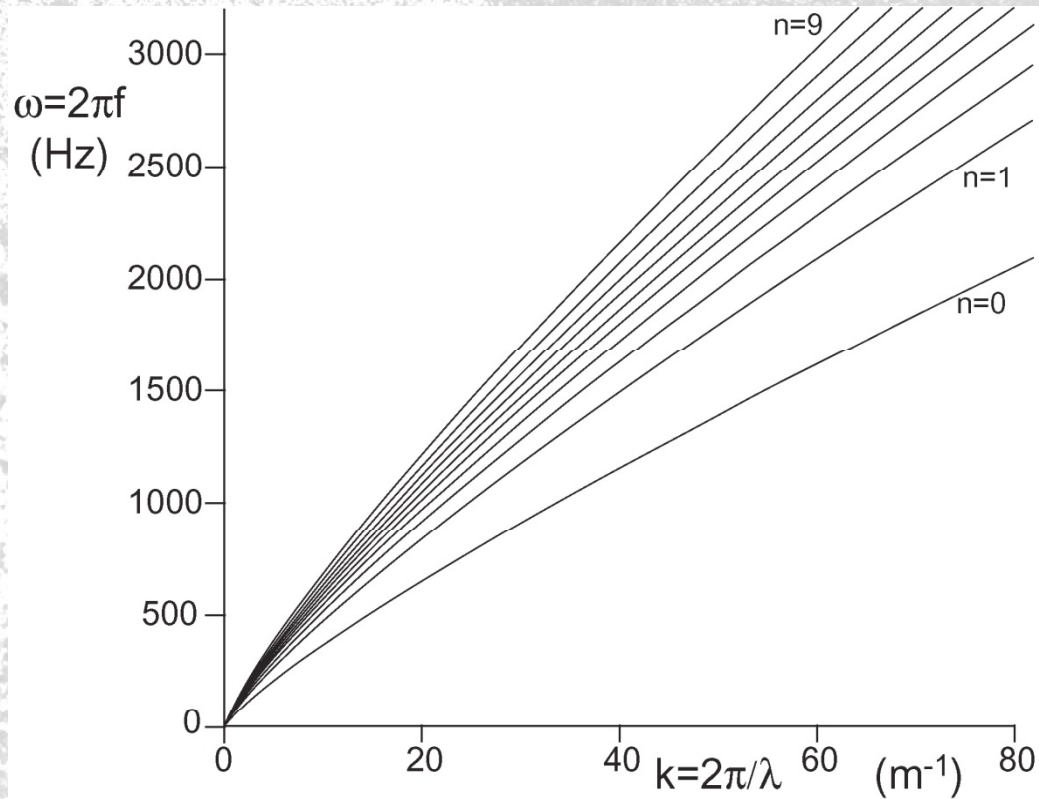
# Dispersion relations

Dispersion relation

$$\omega \propto \left( \frac{E}{\rho} \right)^{1/3} g^{1/6} k^{5/6}$$

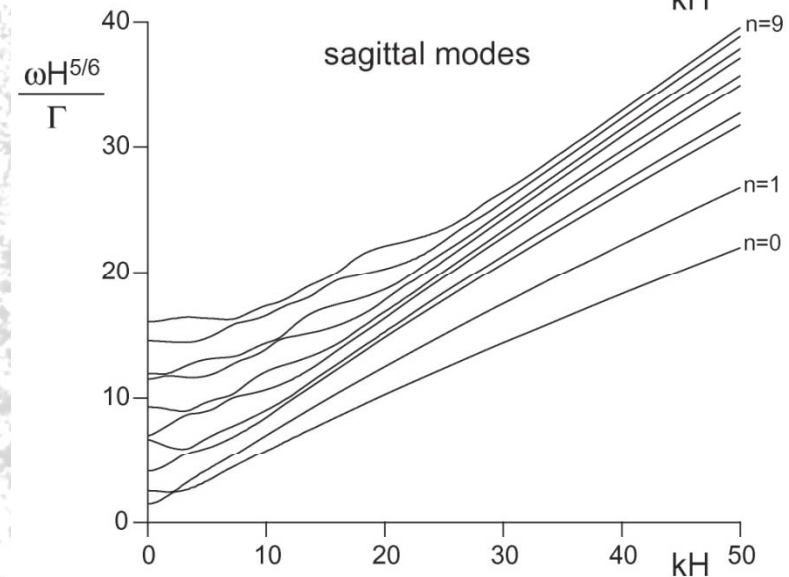
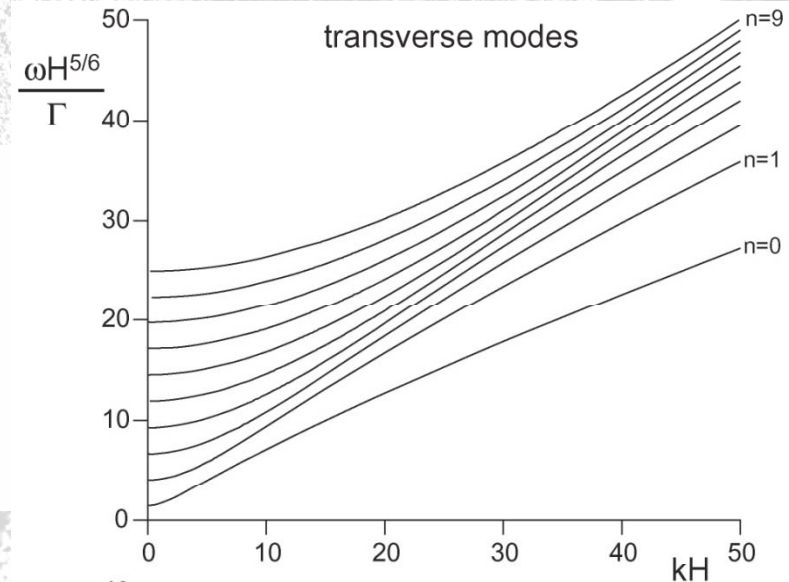
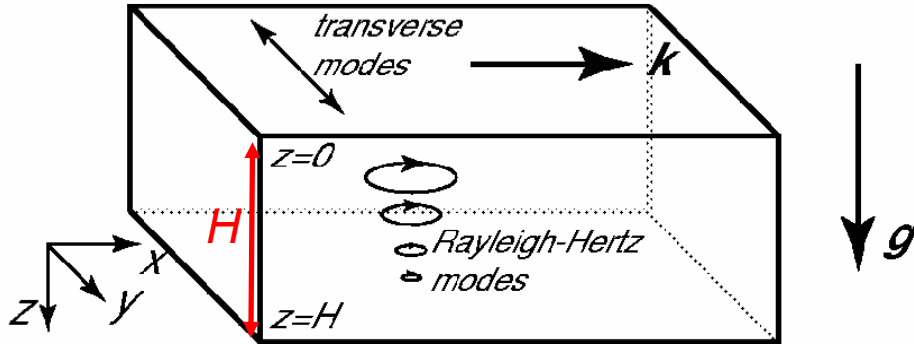
$$P = \rho g (n\lambda)$$

$$c \propto (n\lambda)^{1/6}$$



# Finite size effects

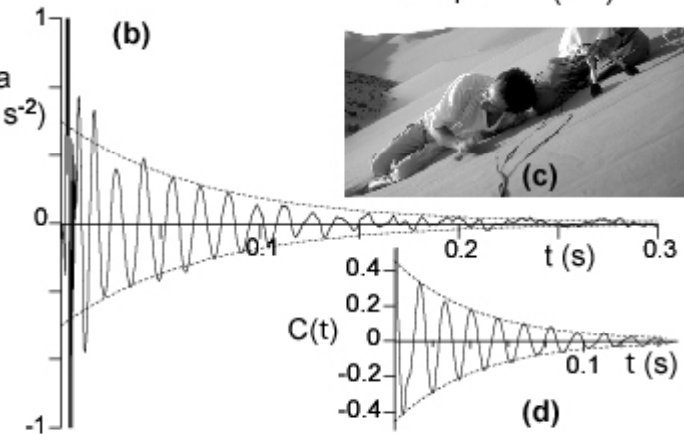
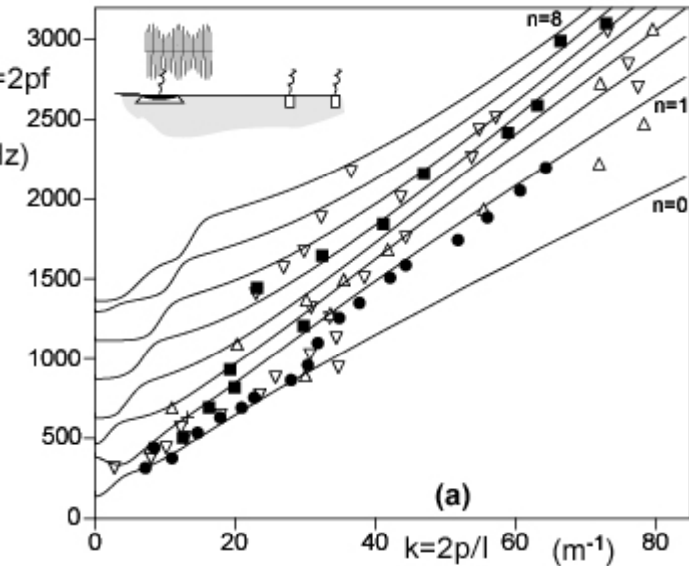
Finite depth :  $H$



Wave guide cut-off

$$\omega_c \propto H^{-5/6}$$

# Reinterprétation of field measurements



$$\Gamma = 50 \text{ s}^{-1} \text{ m}^{5/6} \quad (\Gamma_{MF} = 106 \text{ s}^{-1} \text{ m}^{5/6})$$

$$\omega_c = 2\pi 73 \text{ Hz}$$

Wet sand layer at  $H_0=50\text{cm}$

- Multiplicity of modes !!

# Laboratory scale surface wave propagation

Bonneau et al. PRL **101**, 118001 (2008)

- Can we observe surface wave propagation in the lab ?
- Difficulties (multiplicity of modes – packing preparation)
- Exploration of the vanishing pressure limit (jamming)

# Experimental set-up

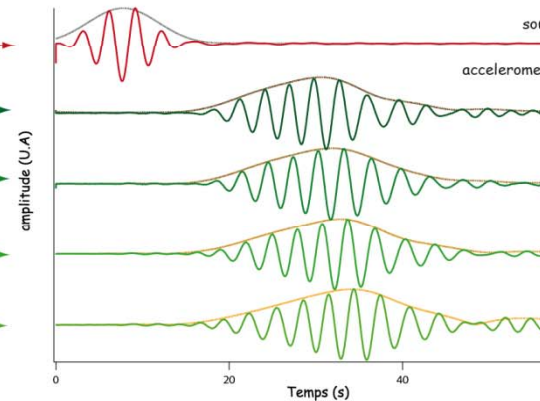
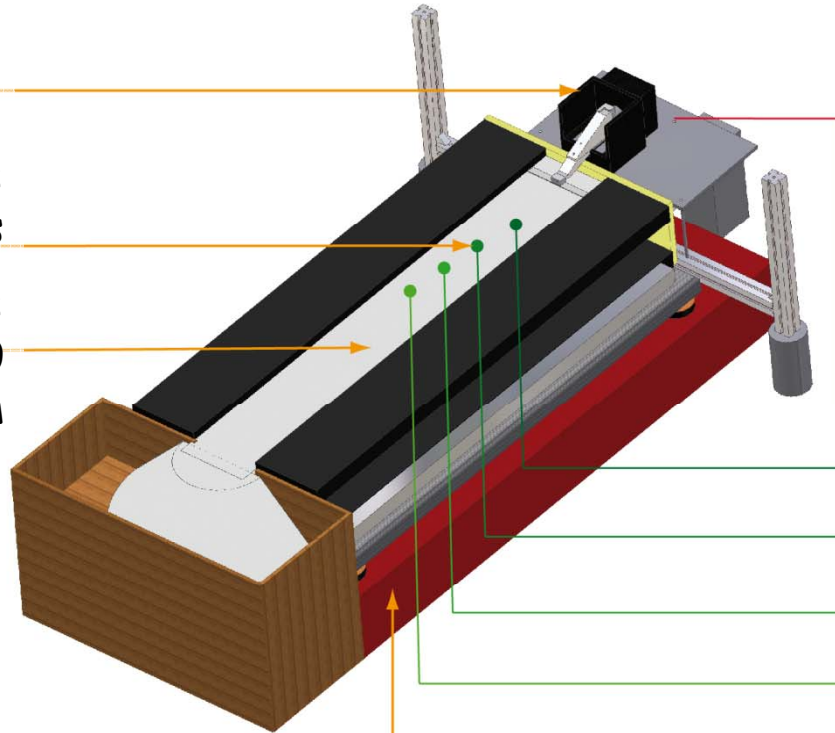
## Longitudinal waves generation

Electromagnetic transducer without spring coupling

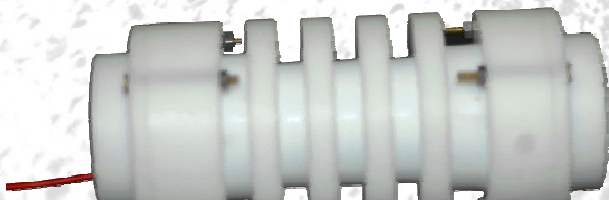
Sensors :  
Accelerometers

Granular medium :  
glass beads  $d \sim 150 \mu\text{m}$

Ground vibration isolating support

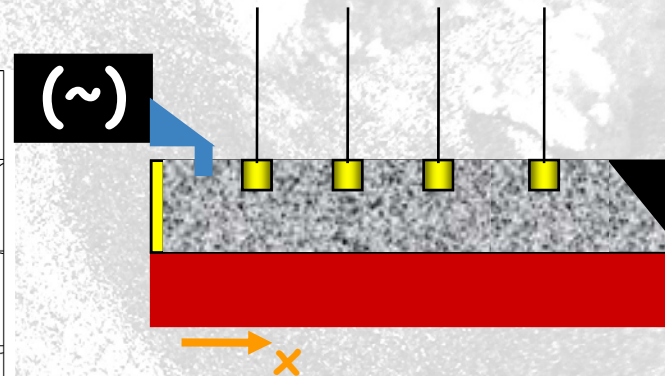
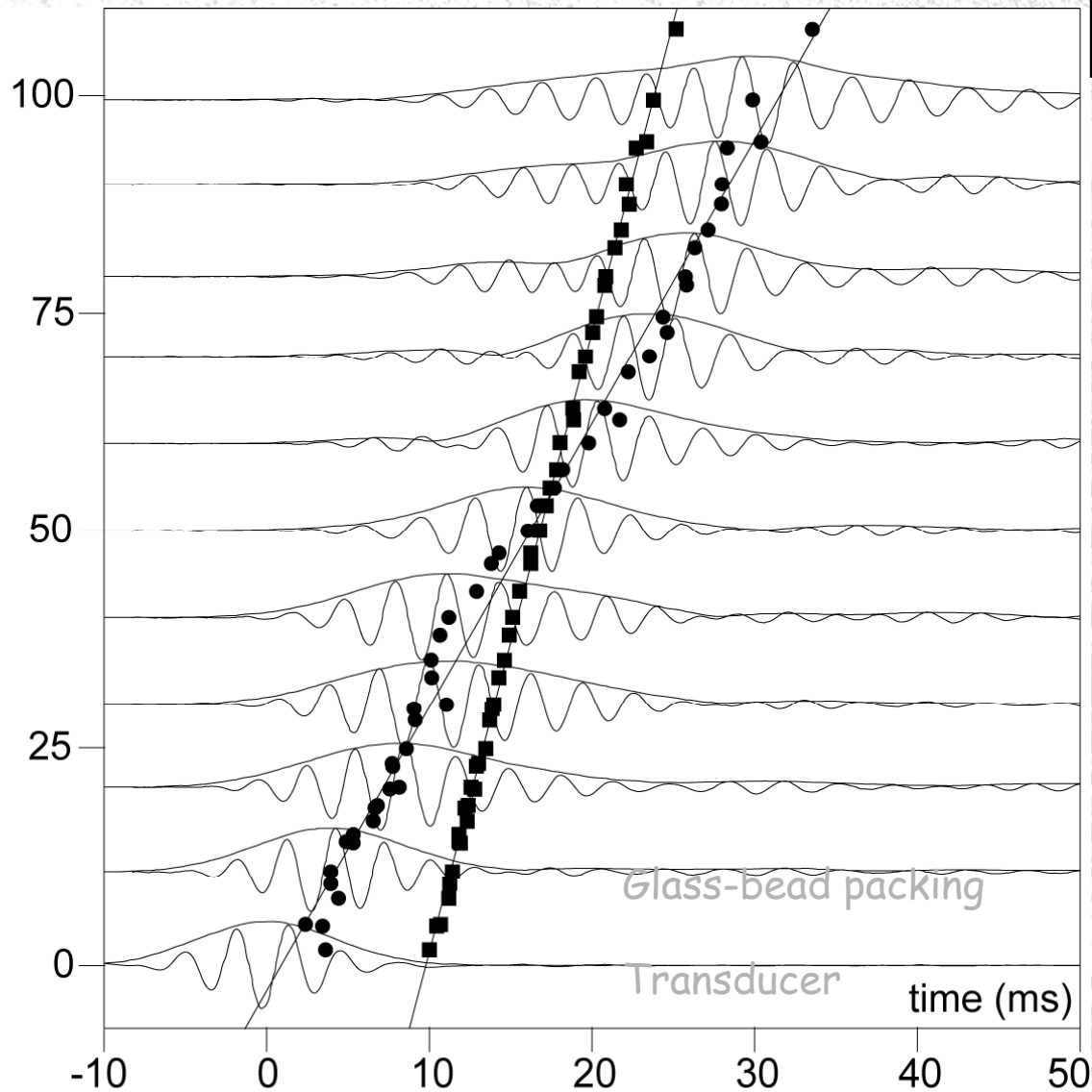


## Transverse waves generation



To avoid grain scale heterogeneities :  
grain size  $\ll$  sensors size

# Wave propagation

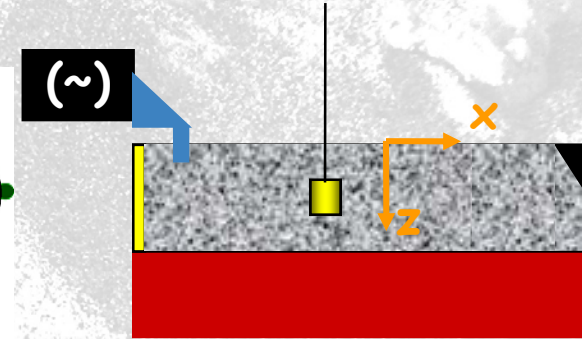
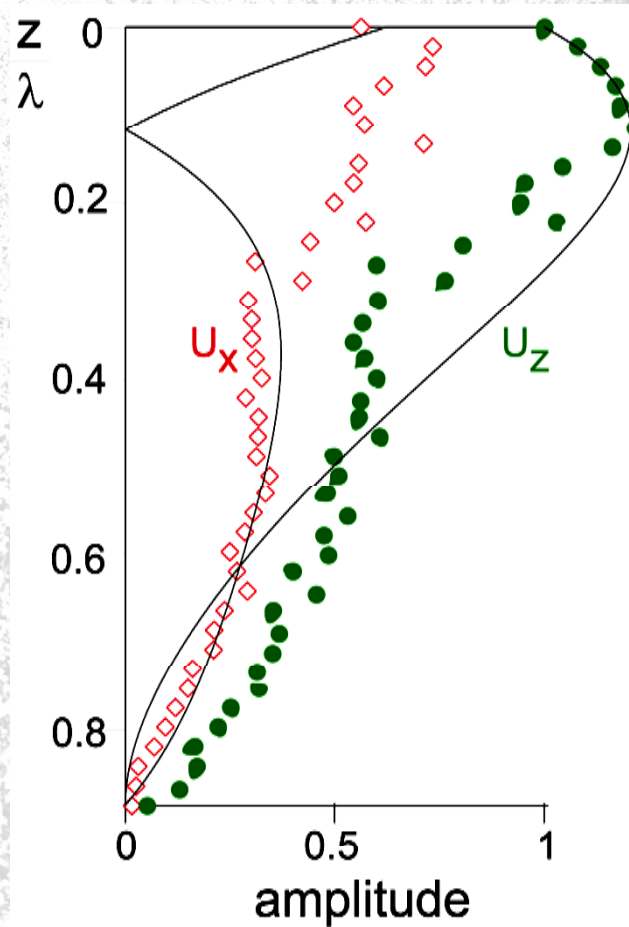
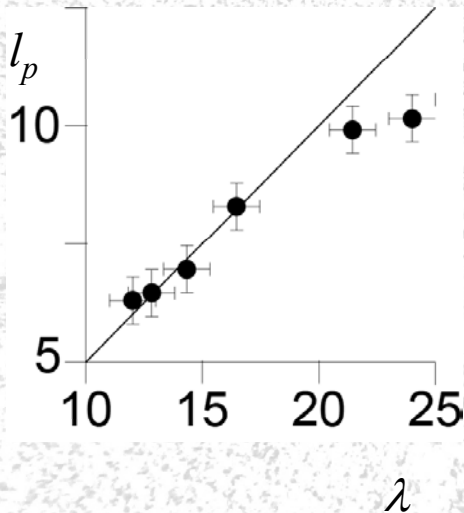


Sagittal waves :  $f = 315\text{Hz}$  :

- Phase velocity :  $72.9\text{ m/s}$
- Group velocity :  $31.2\text{ m/s}$

# Surface waves

$$l_p \cong \lambda / 2$$



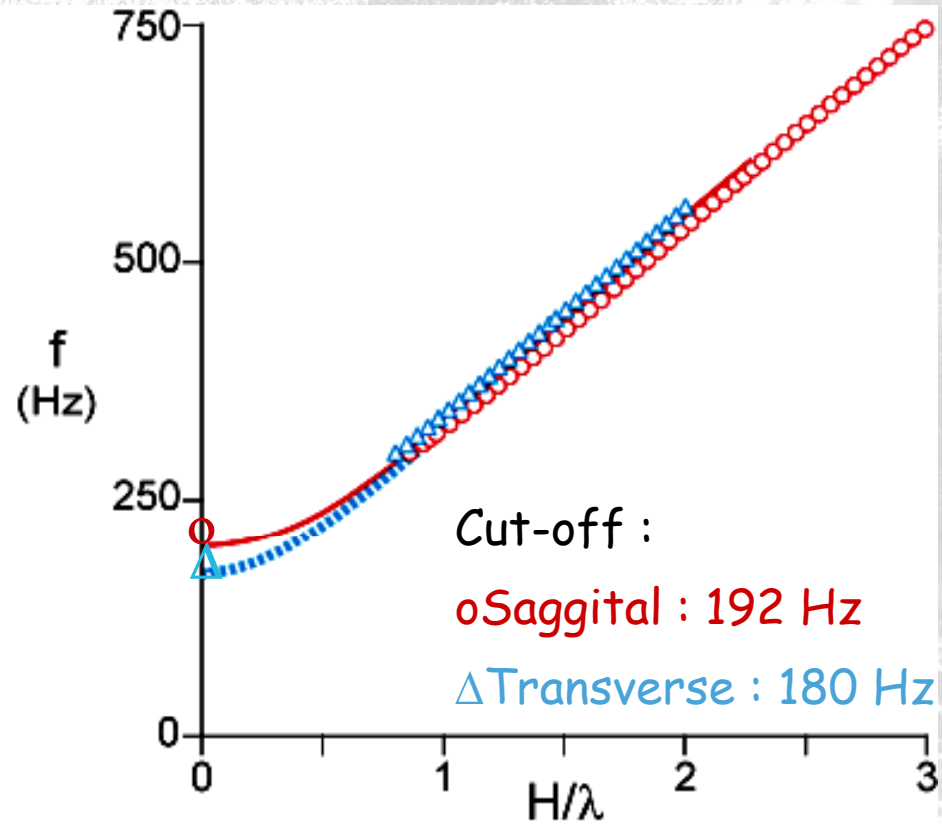
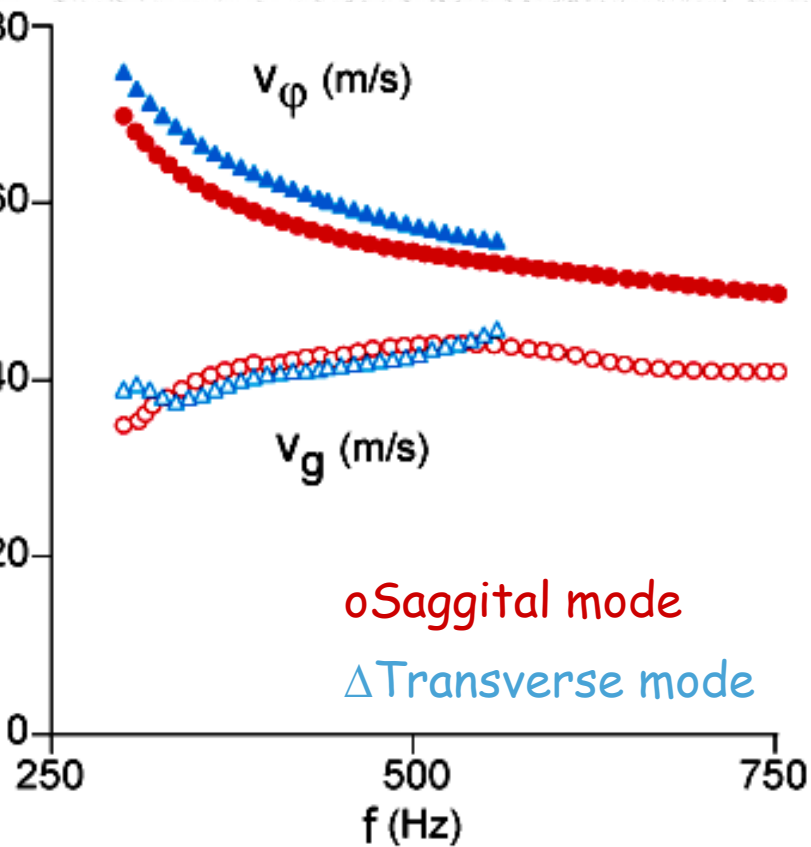
Sagittal waves :

◇ Axial component

• Vertical component

- Waves localized at the surface
- Channel geometry selects the lowest propagation mode

# Experimental dispersion relations



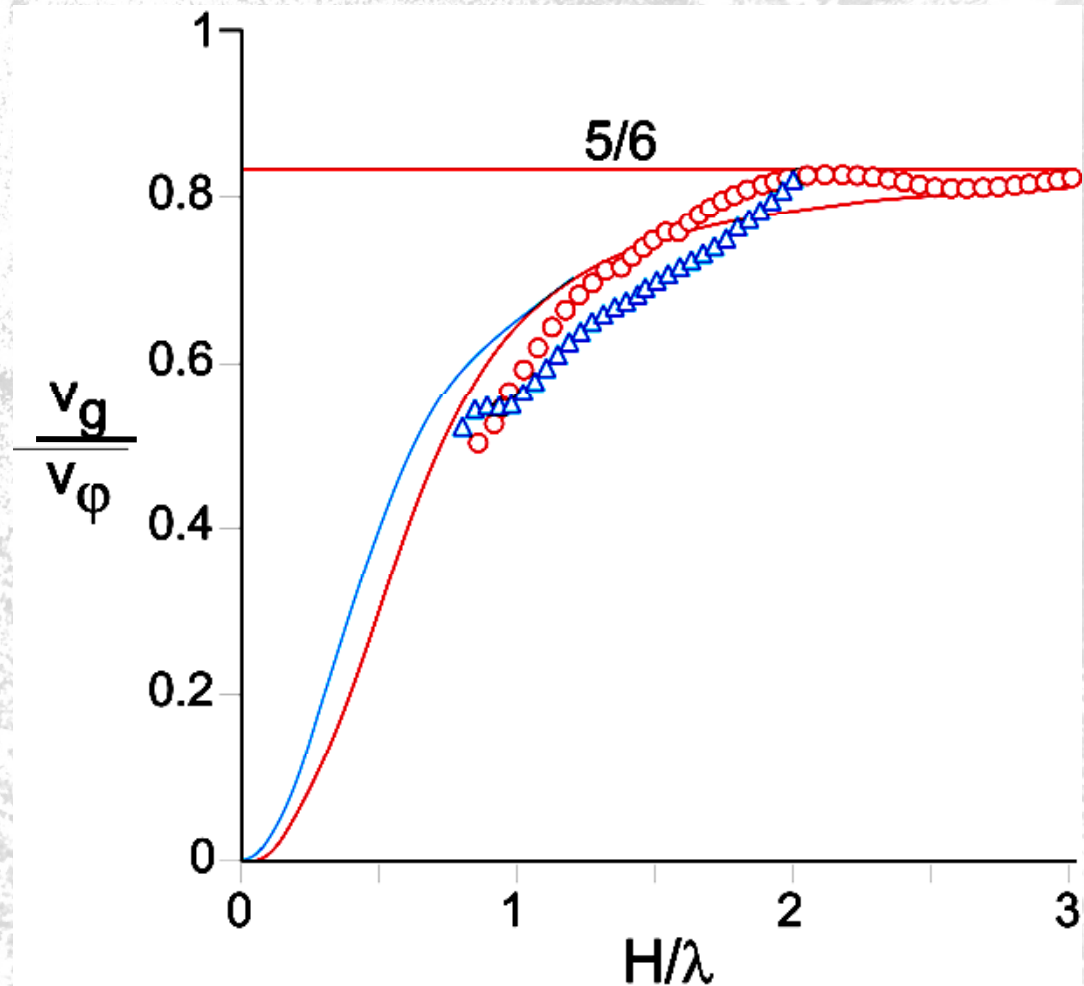
- Transverse and sagittal dispersion relations are matching !



# A test of Hertz scaling

$$\omega \propto k^\alpha \Rightarrow \frac{V_g}{V_\phi} = \alpha$$

$$\text{Hertz} \quad \frac{V_g}{V_\phi} = \frac{5}{6}$$



• Hertz contact law relevant down to very low confining pressure ( $P_0 \cong 10^2 \rho g d \cong 210^2 Pa$ ), however...

# Mean-field failure

Dispersion relations

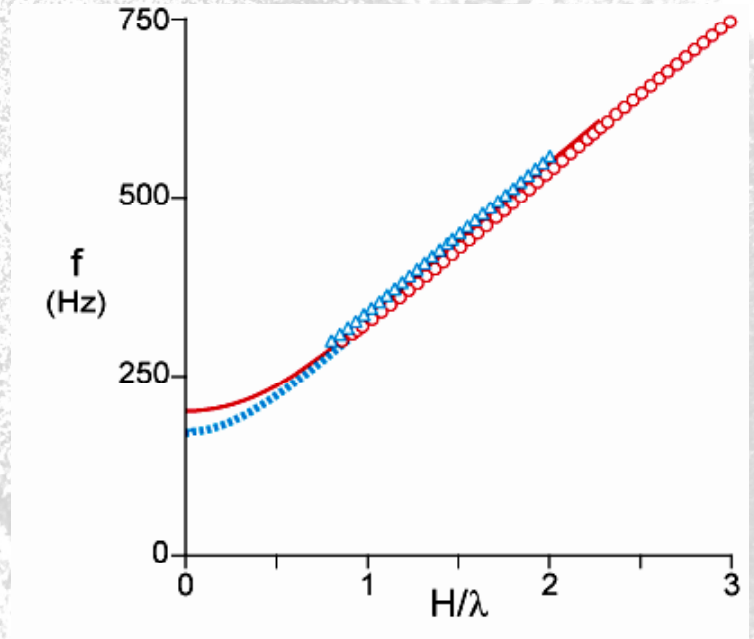
Transverse mode

$$\omega = F_{trans}(A, B, k)$$

Sagittal mode

$$\omega = F_{sagg}(A, B, k)$$

$$A < \frac{B}{5} \Rightarrow F_{trans} \approx F_{sagg}$$



Experiment

$$A^{1/2} B^{-1/6} \approx 0.23$$

Mean-field theories

Frictionless grains

$$A^{1/2} B^{-1/6} \approx 0.44$$

Infinite friction

$$A^{1/2} B^{-1/6} \approx 0.61$$

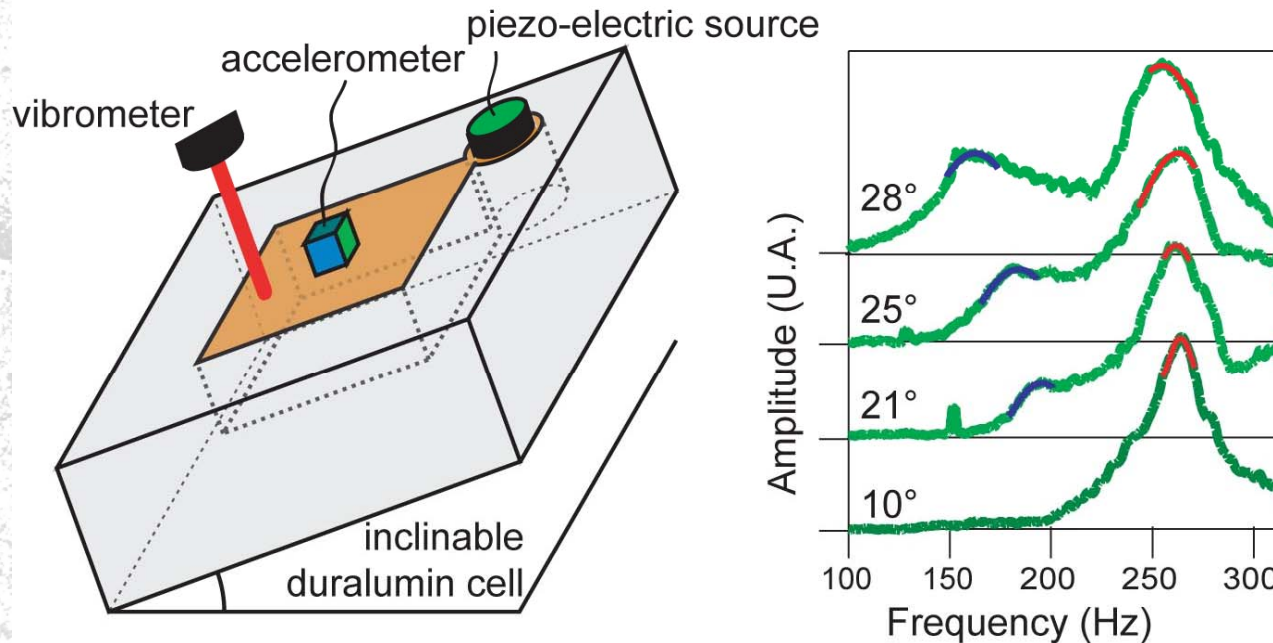
- Shear stiffness 3.5 to 7 times smaller than mean-field predictions !

# Summary and Conclusions

- **In a granular packing under gravity**
  - Acoustic perturbations travel as surface waves
  - Waveguide feature of the channel setup selects the fundamental mode
  - Obtained transverse and sagittal fundamental mode dispersion relations for a glass-beads packing
  - Hertz non-linear scaling is consistent with our measurements
  - Mean-field fails for determining the elastic constants
- **New issues**
  - Shear modulus weakness ?
  - How to measure independently A and B (new experimental configuration)
  - The non-linear high amplitude regime ?

# Approach to unjamming

## Acoustic resonance study (preliminary results)



Near avalanche onset

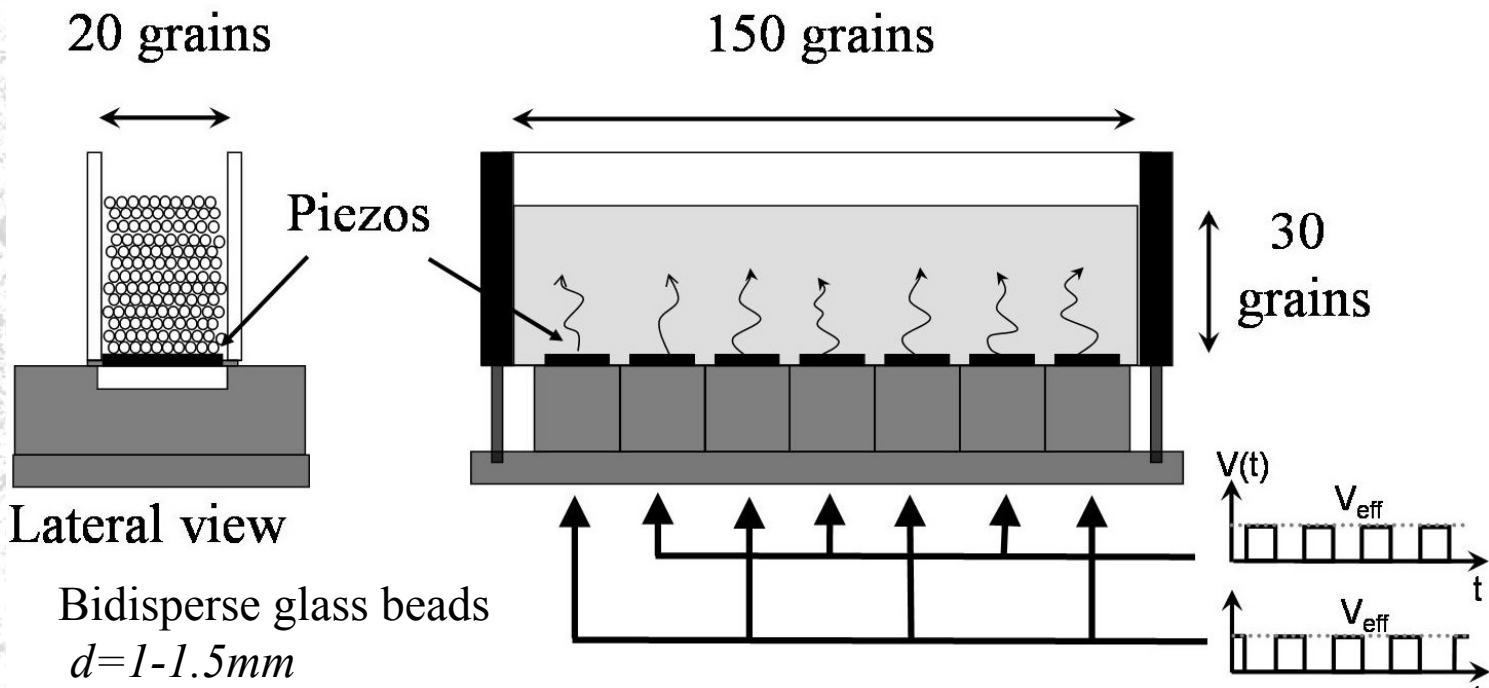
- Stiffness weakening
- Dissipation increases
- « Soft-modes » signature?

# Sono-fluidization of granular packing

*With Gabriel Caballero C.I.M.A. Monterey Mexico*

Ref. Caballero, Clément *preprint Cond-Mat* 0907.0317v2 (2009)  
Caballero et al. *Powder and Grains*, p 339 (2005)





Frequencies :  $300\text{ Hz} < f < 1000\text{ Hz}$

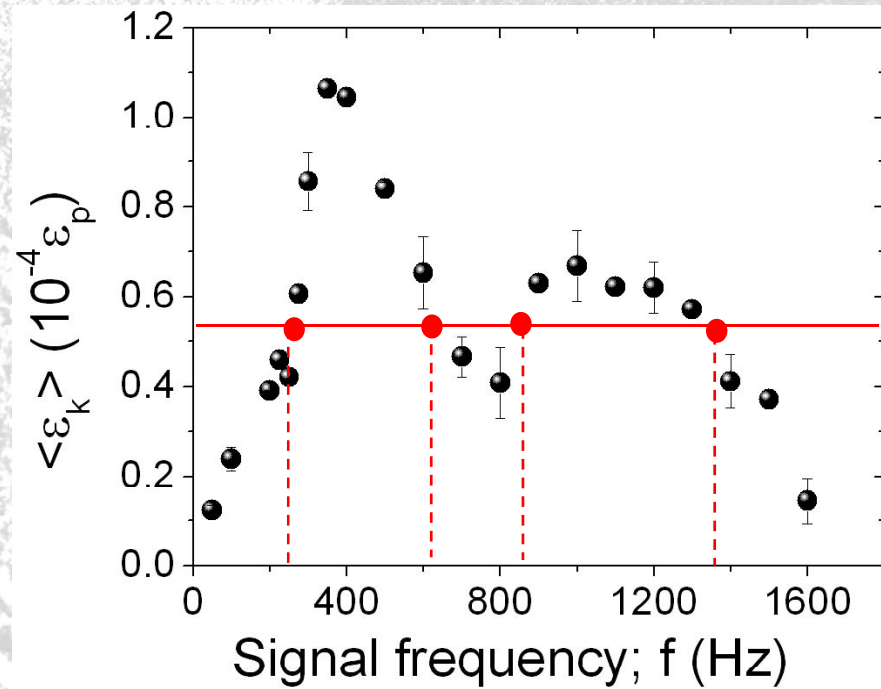
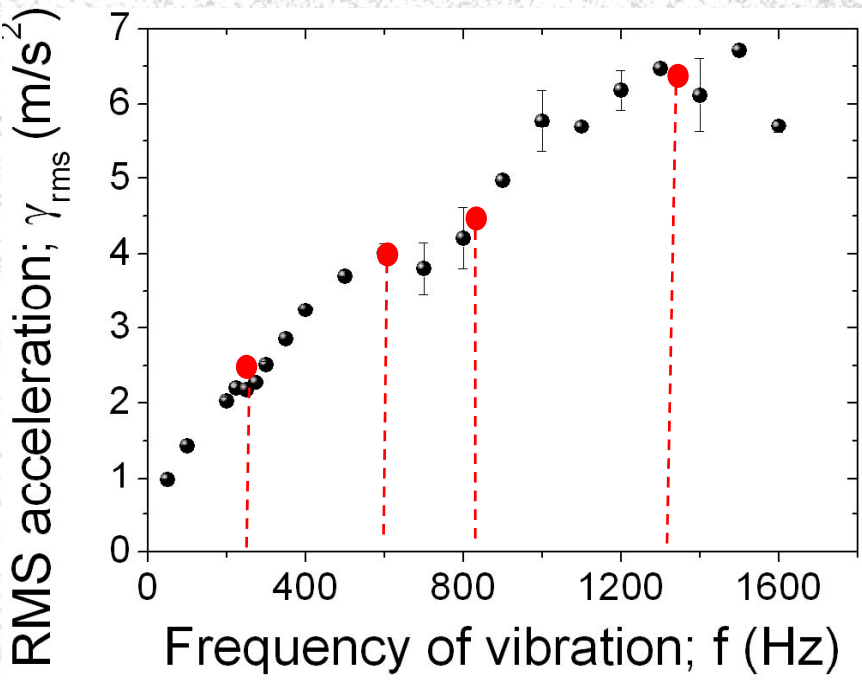
Weak agitation

$$\langle \varepsilon_k \rangle < 10^{-4} \rho g d$$

$$\gamma < g$$

# Acceleration and energy vs driving frequencies

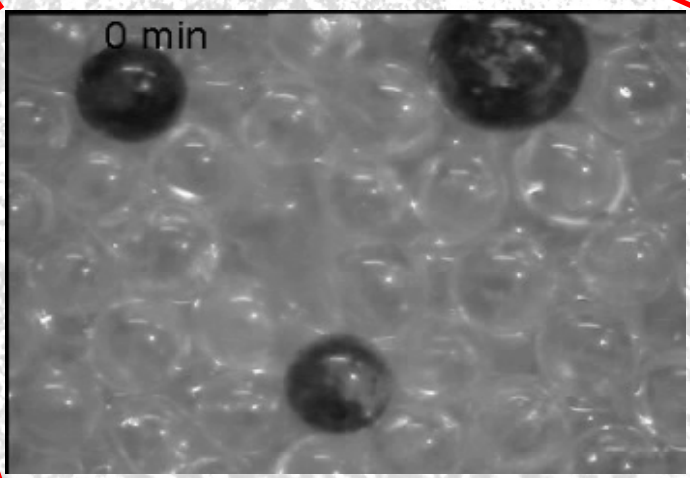
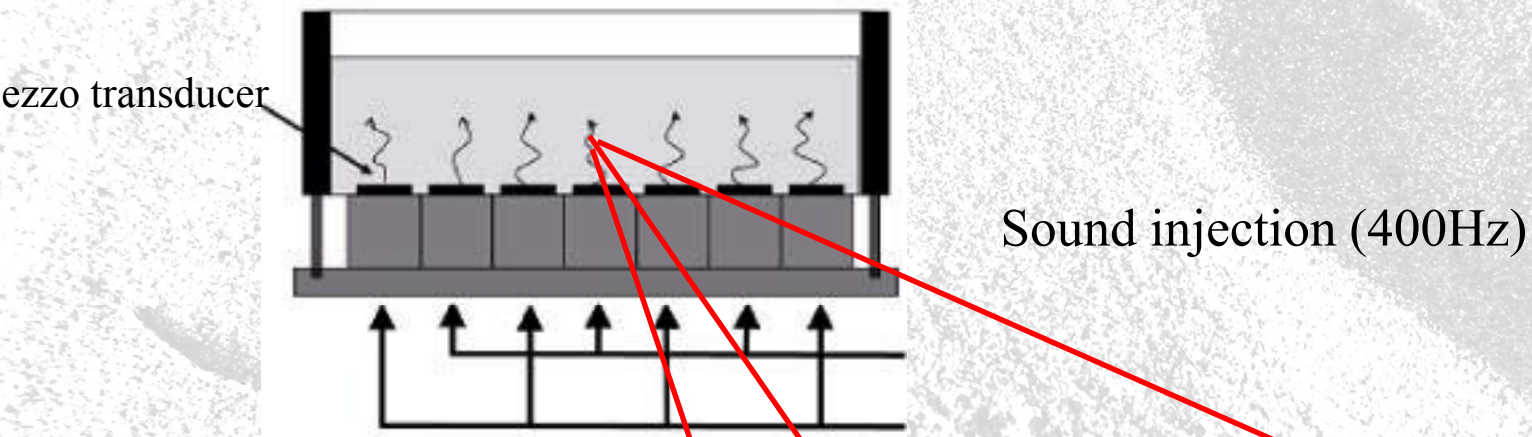
Constant  $V_0 = 10V$



$$\gamma_{rms} < g$$

$$\langle \epsilon_k \rangle \ll \epsilon_p$$

# Sono-fluidization



1 image/min

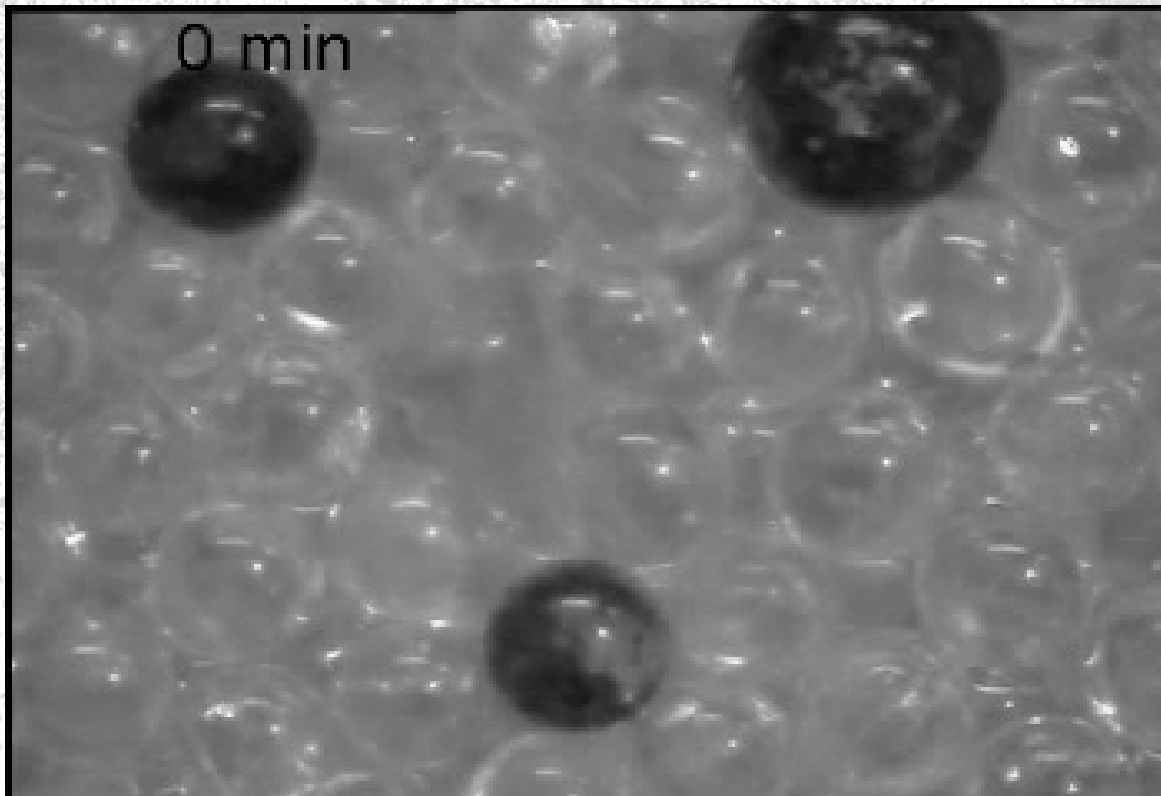


# Microscopic dynamics

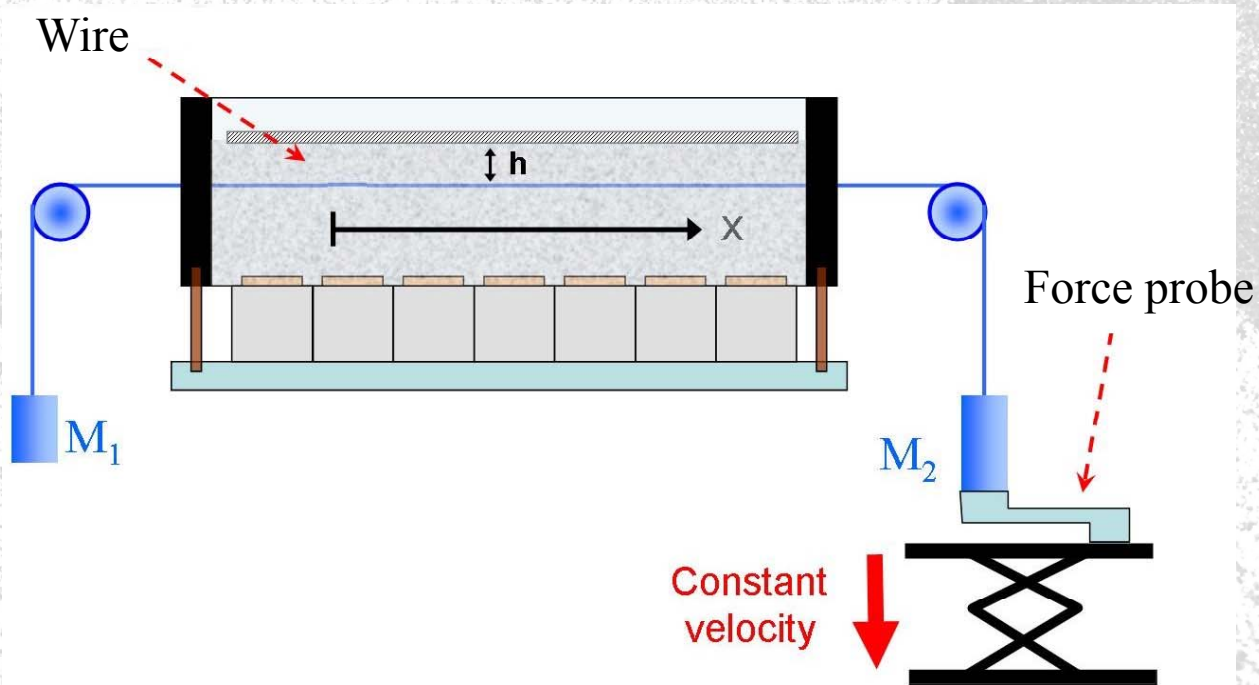
One image each 3 minutes

$$F = 400\text{Hz}$$

$$\gamma_{rms} = g/3$$

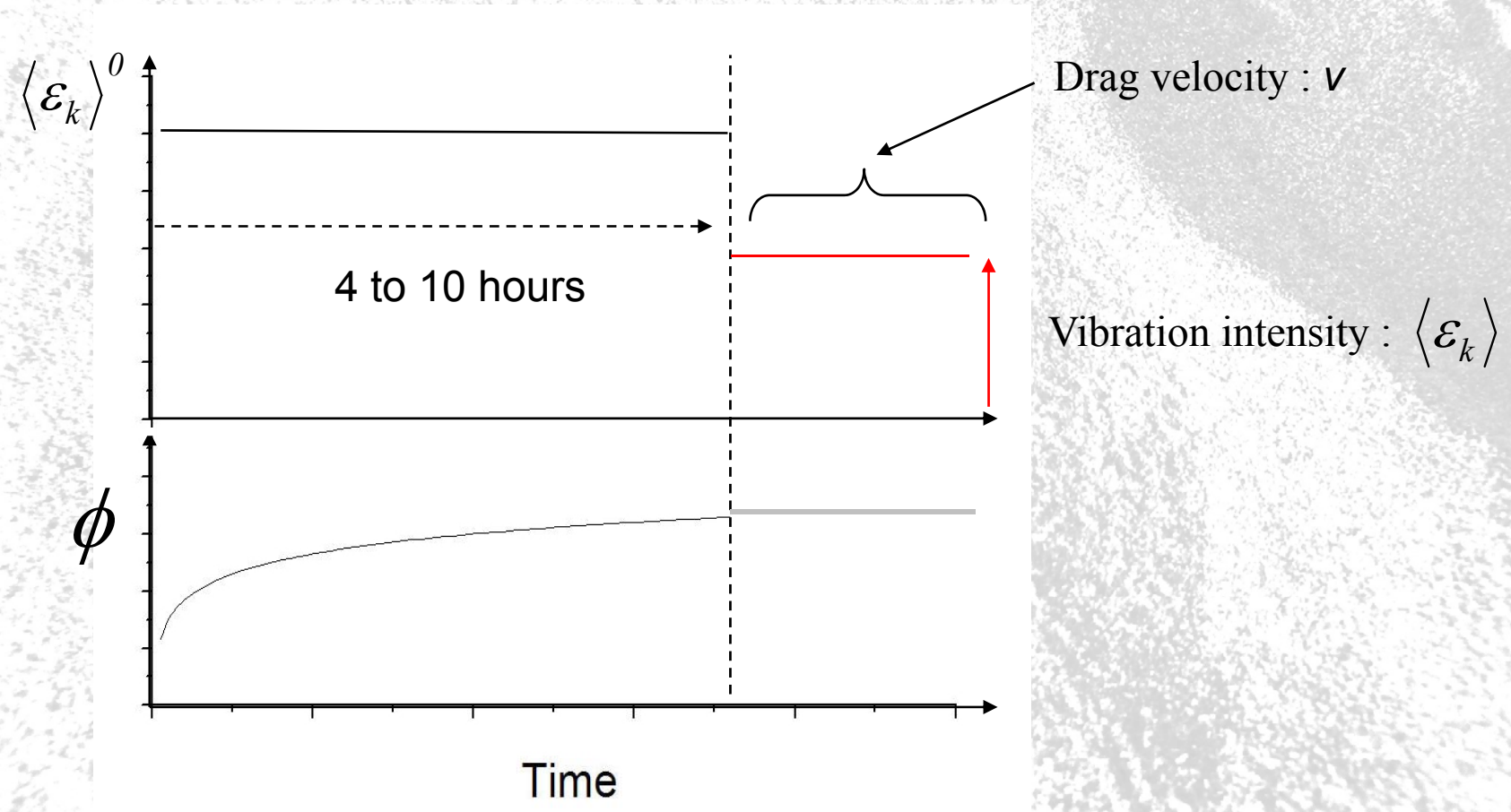


# Drag force experiments

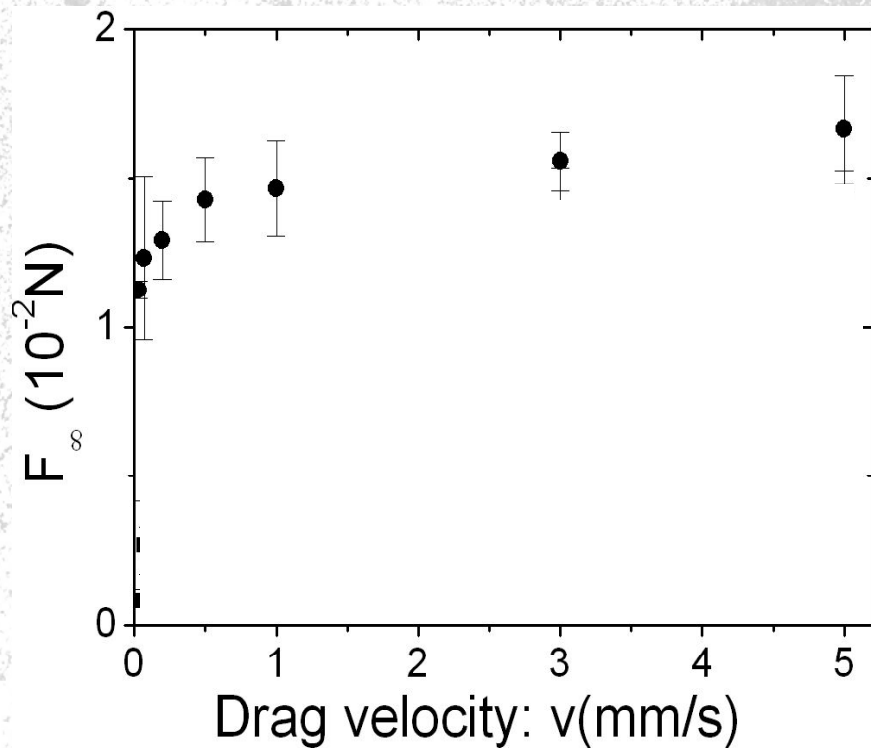


Metallic wire :  $e=0.1\text{mm} < d=1\text{mm}$

# Protocol and control parameters



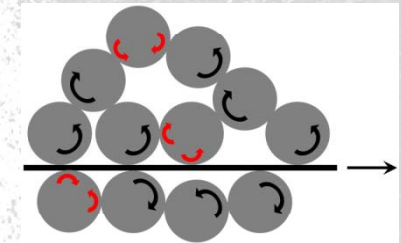
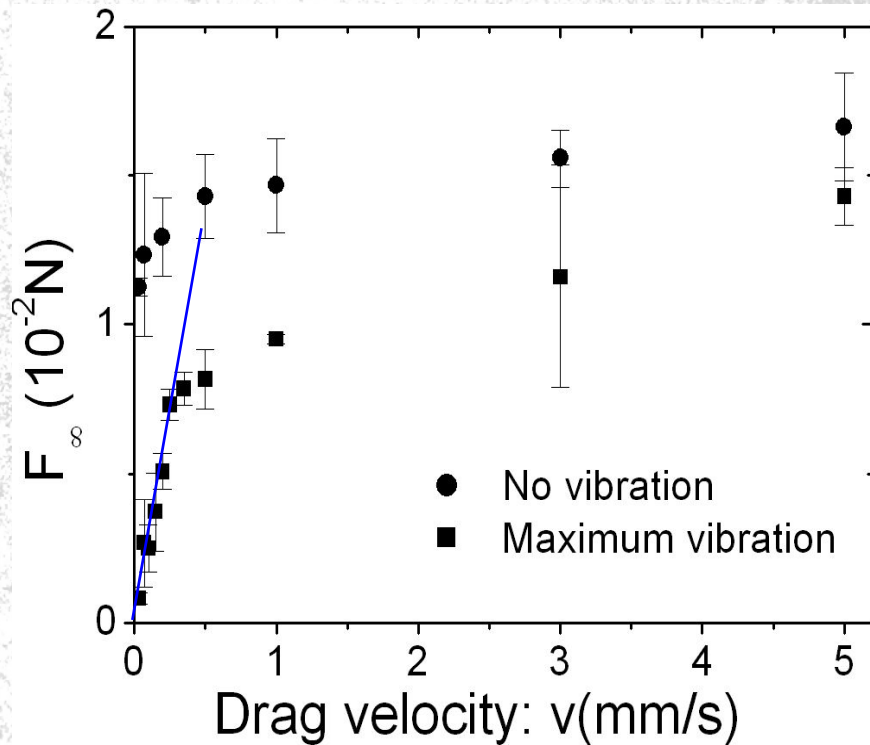
# Drag force on the thread



- No vibration

$$F \cong F_0 + A \ln(V / V_0)$$

# Drag force on the thread



- Low driving velocity

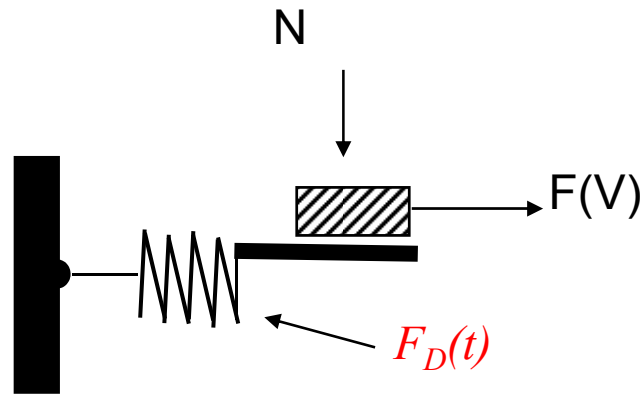
A linear regime :

$$F \propto V$$

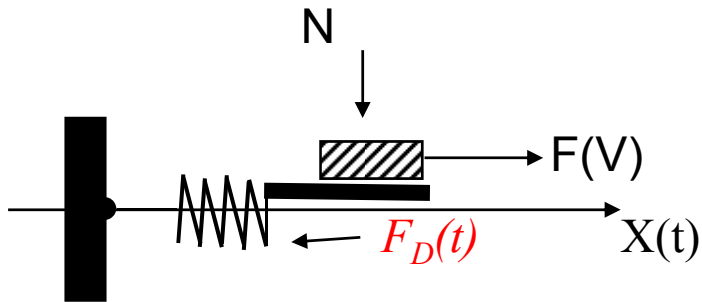
Viscosity ?

# A simple heuristic model

## Elasticity/friction



- Explain dynamic stress threshold vanishing ?
- Explain  $F \propto V$  ?



Constant  $V$  block driving  
 $\mu$  friction  
 $\omega_0$  spring resonance pulsation  
 $M$  spring mass

$F_D = M G(t)$  driving force on the spring

$G(t) = G_0 \sin 2\pi f_D t$  harmonic driving

Adimensionalisation parameters

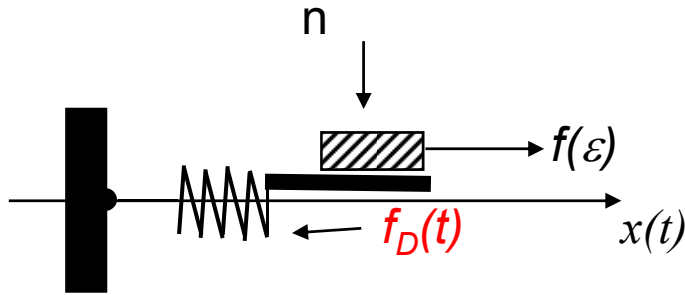
$$F_0 = \mu N$$

$$t_0 = 1 / \omega_0$$

$$V_0 = \frac{\mu N}{M \omega_0}$$

$$X_0 = \frac{\mu N}{M \omega_0^2}$$

Dimensionless driving velocity



$$\varepsilon = \frac{V}{V_0}$$

Eq. of motion  $\ddot{x} = -x + \tilde{f} - \tilde{f}_D$

Sliding  $\tilde{f} = \text{sgn}(\varepsilon - \dot{x})$

Sticking  $\dot{x} = \varepsilon, \tilde{f} = x - \tilde{f}_D$

$$\tilde{f}_D = \gamma_D \sin \omega_D \tau$$

Harmonic driving

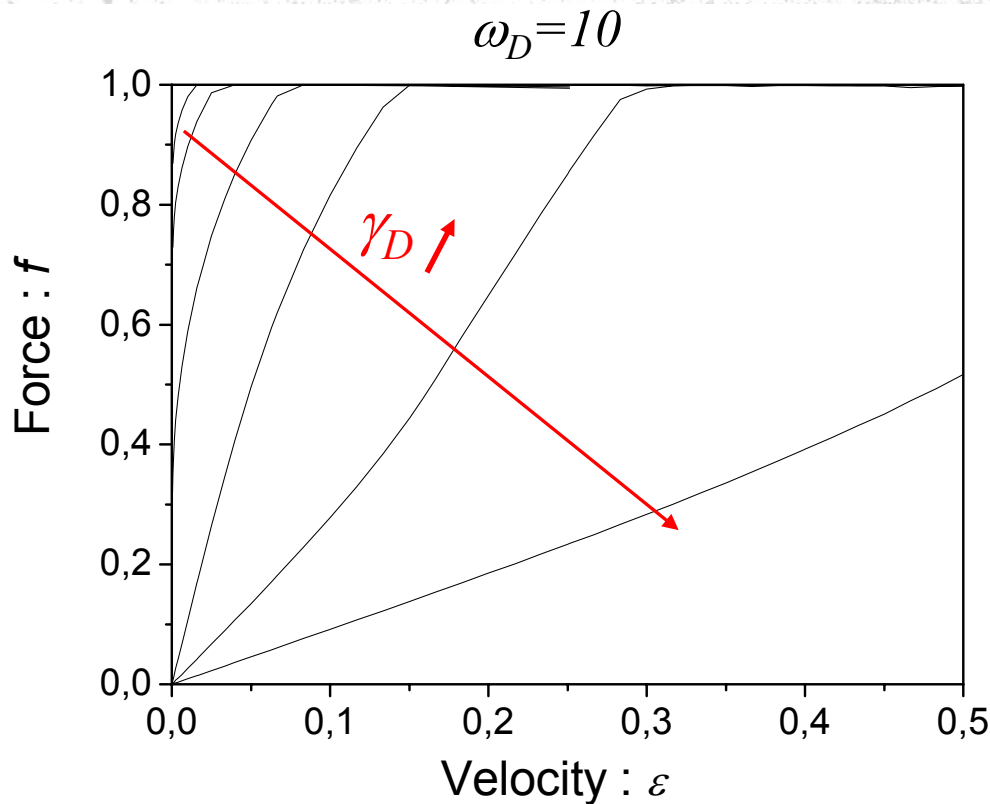
• Numerical solution :  $\bar{f}(\varepsilon)$  for varying  $\gamma_D$  the driving amplitude

• Exact results when  $\varepsilon \gg 1$   $\bar{f}(\varepsilon) \rightarrow 1$

when  $\gamma_D \gg 1$   $\bar{f}(\varepsilon) = \frac{2}{\pi} \frac{|\omega_D^2 - 1|}{\omega_D} \varepsilon \propto \varepsilon$



# Mean drag force $\bar{f}(\varepsilon)$



$$\gamma_D = \frac{MG_0}{\mu N}$$

$$\tilde{f}_D = \gamma_D \sin \omega_D \tau$$

- Weakening with driving amplitude

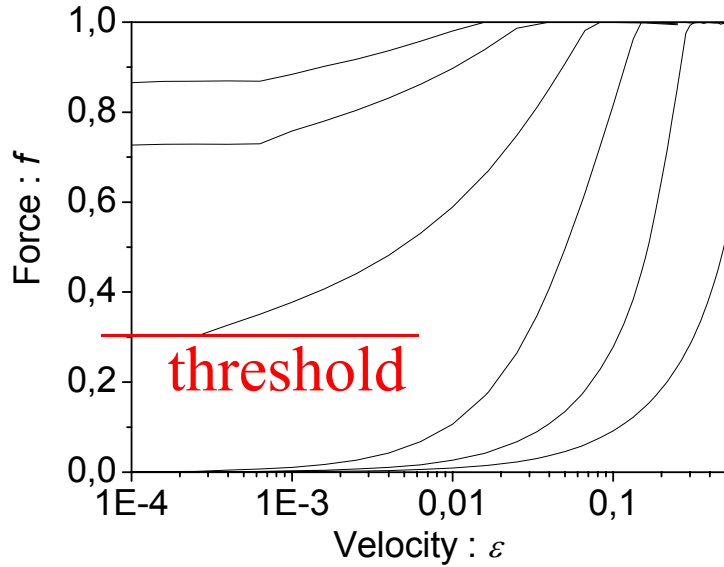
$$\bar{f}(\varepsilon) \downarrow \text{ when } \gamma_D \uparrow$$

- Hardening rheology

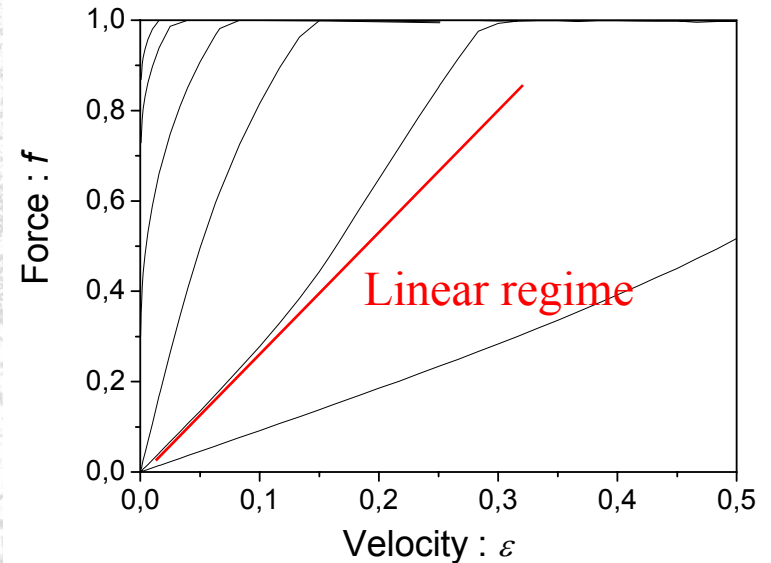
$$\bar{f}(\varepsilon) \uparrow \text{ when } \varepsilon \uparrow$$

# Mean drag force $f(\varepsilon)$

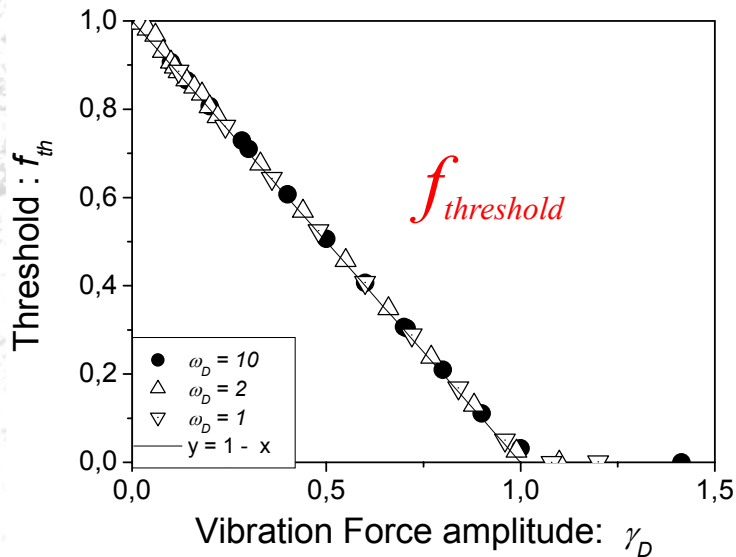
Low amplitude driving



Large amplitude driving



$\omega_D = 10$



- if  $\gamma_D < 1$ , threshold,  $\mu_{th} = \mu(1 - \gamma_D)$
- if  $\gamma_D \geq 1$ , linear regime

$$F \propto \mu \frac{V}{\delta V} N$$

$\delta V$  rms velocity fluctuations

## Summary on the model outcome

- Simple heuristic model (internal elastic modes / solid friction)
- Drag resistance decreases with driving intensity
- Stress hardening (no  $\ln V$  regime)
- Low driving intensity : threshold friction force at low  $V$
- Large driving intensity : linear relation  $F \approx \mu N \frac{V}{\delta V}$

Experimentally

$$\mu_{eff} = \frac{F}{N} = \alpha \frac{V}{\delta V}$$

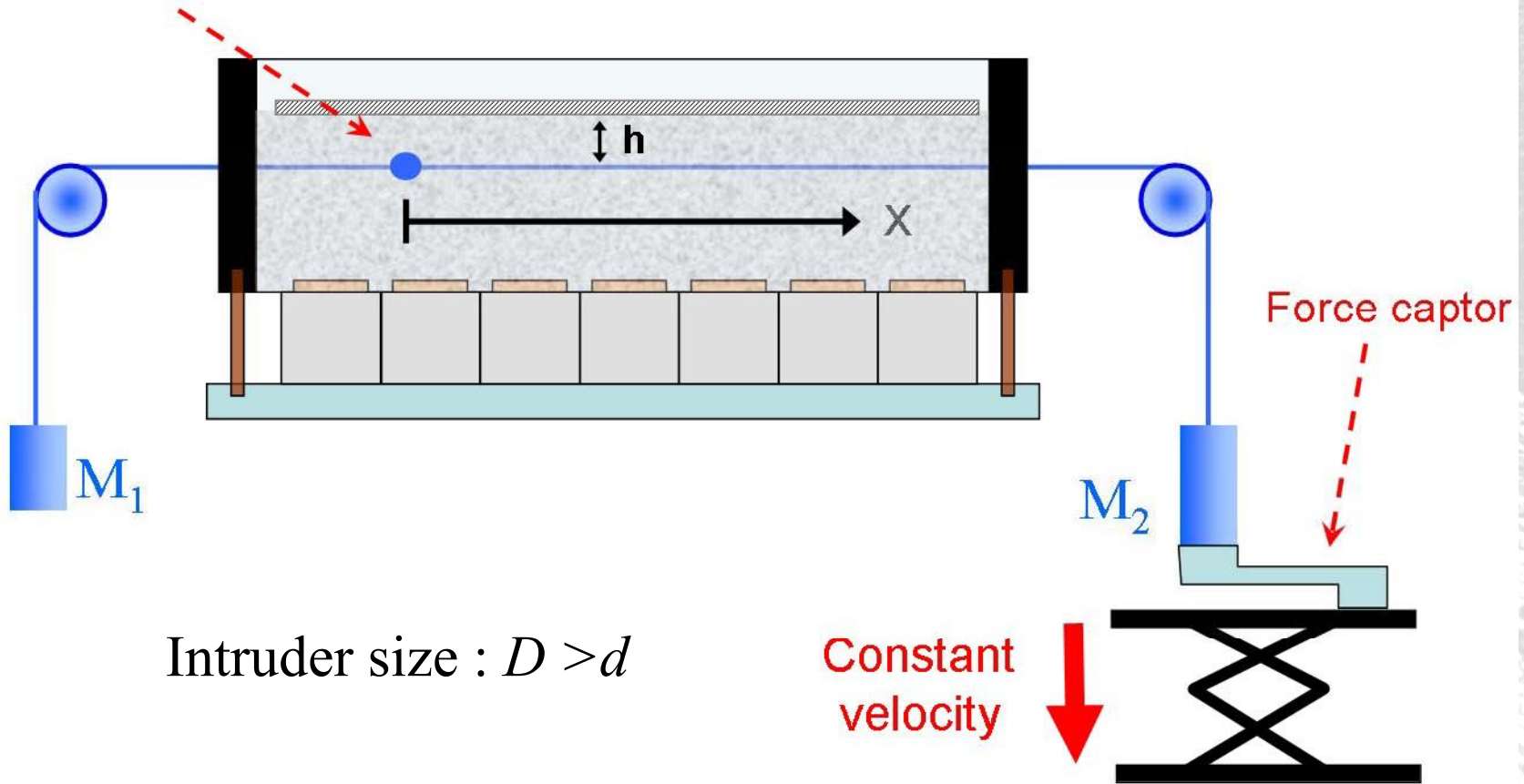
$\delta V$  rms velocity fluctuation

$$\delta V = 1.2 \cdot 10^{-3} \text{ m/s}$$

$$\alpha = 1.3$$

# Drag force on a spherical intruder

Intruder grain

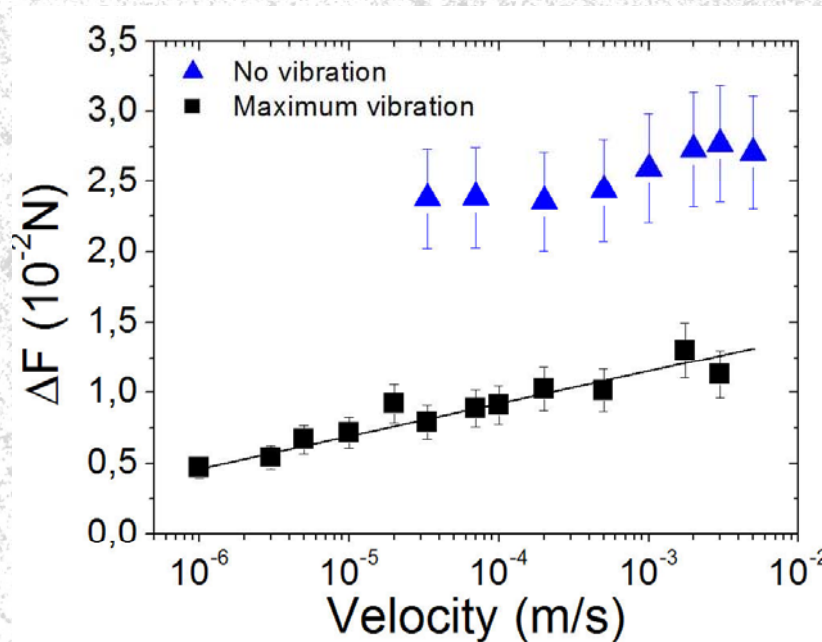


Intruder size :  $D > d$

Constant  
velocity

# Drag force on thread + bead

Bead contribution :  $\Delta F = F_{\infty} - F_{\infty}^{(thread)}$



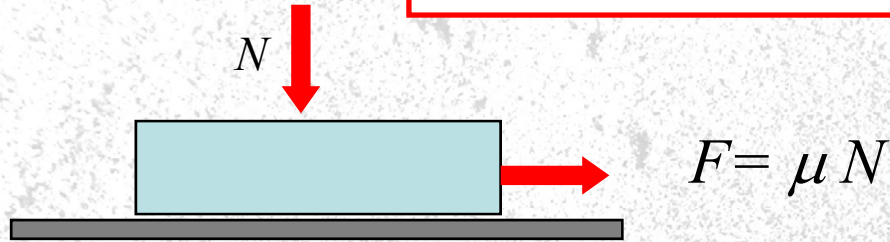
$D=2mm$

No vibration

Vibration

- Stress strengthening
- Threshold at low vibration intensity
- Non linear variation :  $\Delta F \cong \Delta F_0 + B \ln(V / V_0)$

# Solid/solid friction : creeping motion



$$\mu(\lambda, \dot{x}) \propto \mu_0 + B \ln\left(\frac{\lambda}{\lambda_0}\right) + A \ln\left(\frac{\dot{x}}{V_0}\right)$$

$$\dot{\lambda} = 1 - \frac{\lambda \dot{x}}{D_0}$$

$\lambda$  : age of the interface

(Dietrich – Ruina closure)

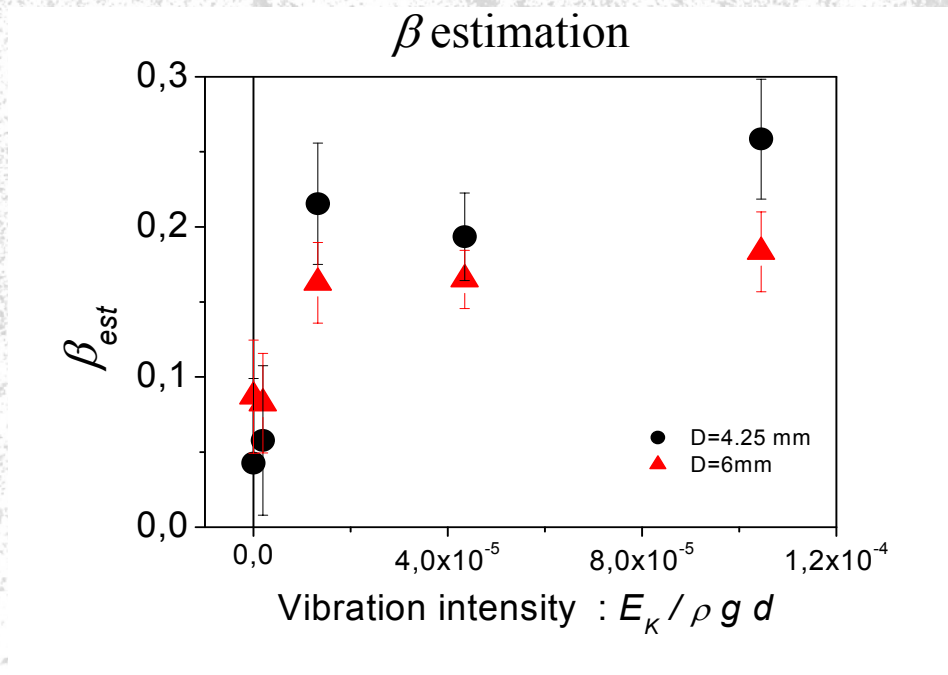
- Stress strengthening/stress weakening regimes
- Pinning/unpinning dynamics
- Thermal activation of the unpinning processes

$$A \propto \frac{k_B T}{\sigma_0 \xi^3}$$

« nano bloc » size  $\xi = 10^{-9} \text{m}$

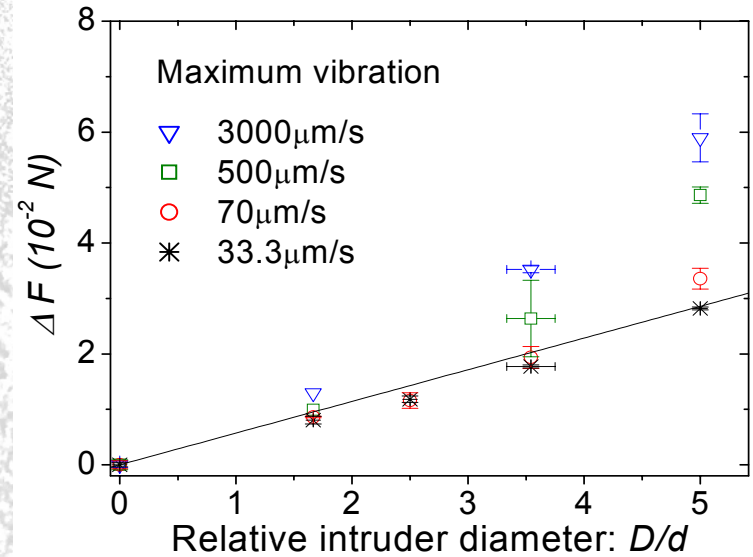
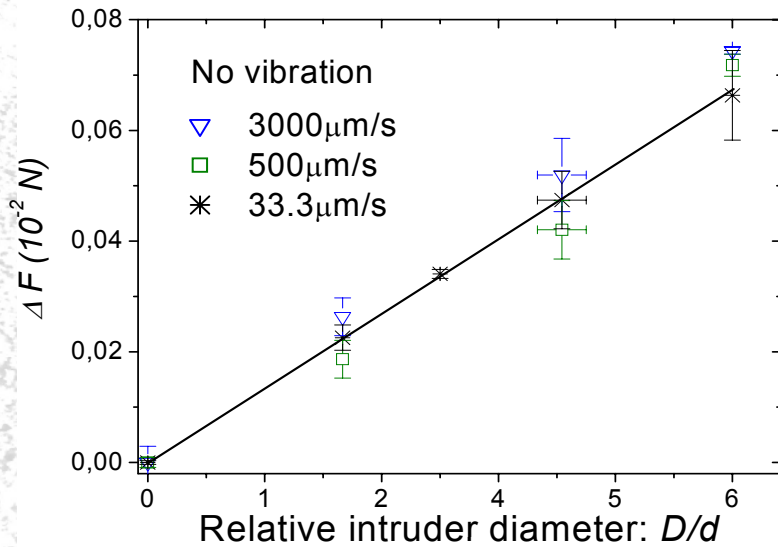
Ex: Baumberger et al. PRB (1999)

$$\mu(v) = \mu(v_{\text{ref}}) + \beta \ln(v/v_{\text{ref}})$$

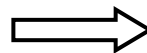


- Weak dependence on kinetic energy

# Intruder size dependence



Without vibration  
With vibration at low  $V$



$$\Delta F \propto D$$

• Anomalous « geometrical hardening »

$$\mu_{eff} \propto D^{-1}$$



# Summary

- Effective friction of a macroscopic intruder decreases with vibration intensity
- Effective rheology displays logarithmic hardening

$$\mu(v) = \mu(v_{\text{ref}}) + \beta \ln(v/v_{\text{ref}})$$

- Effective friction is larger for smaller objects (geometrical hardening)
- Hardening weakly depends on vibration energy

# Spreading of a granular droplet

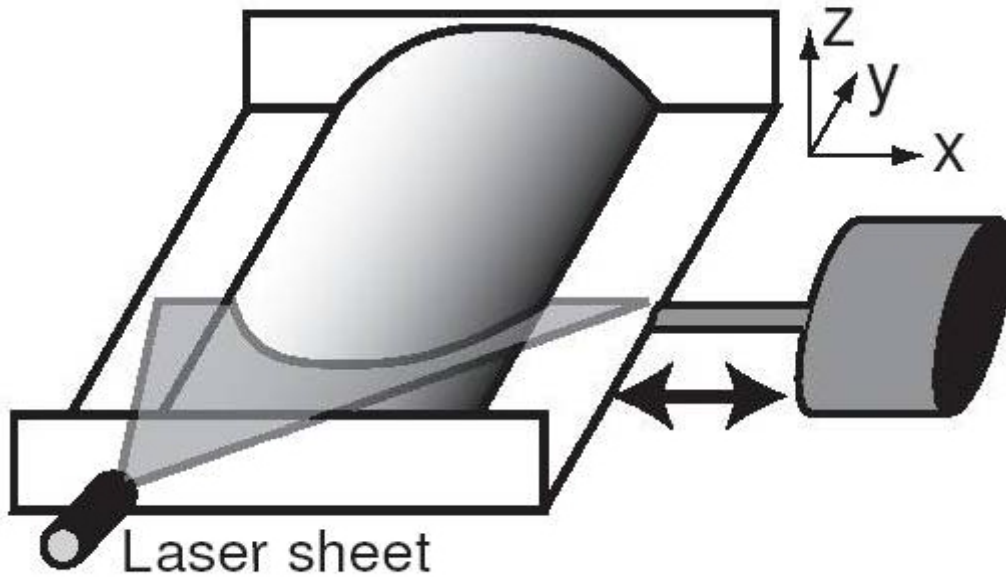
## An inertia tribometer

*With*

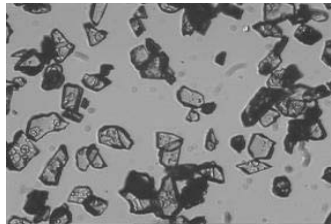
- *Ivan SANCHEZ, Univ. Simon Bolivar-Venezuela*
- *Franck RAYNAUD, José LANUZA, Bruno ANDREOTTI, ESPCI*
- *Igor ARANSON Argonne National Lab*



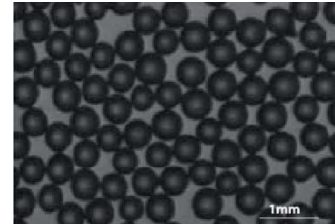
Ref : Sanchez et al, Phys.Rev.E 76, 060301 (2007)



Grains  
 $d=250\mu m$



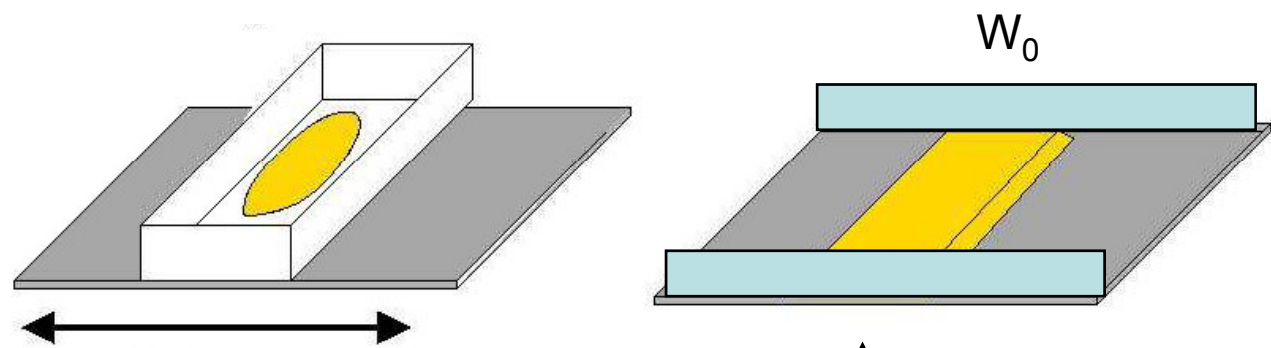
Fontainebleau Sand



Glass beads

Substrate roughness :  $10\mu m \ll d$

# Granular film preparation procedure



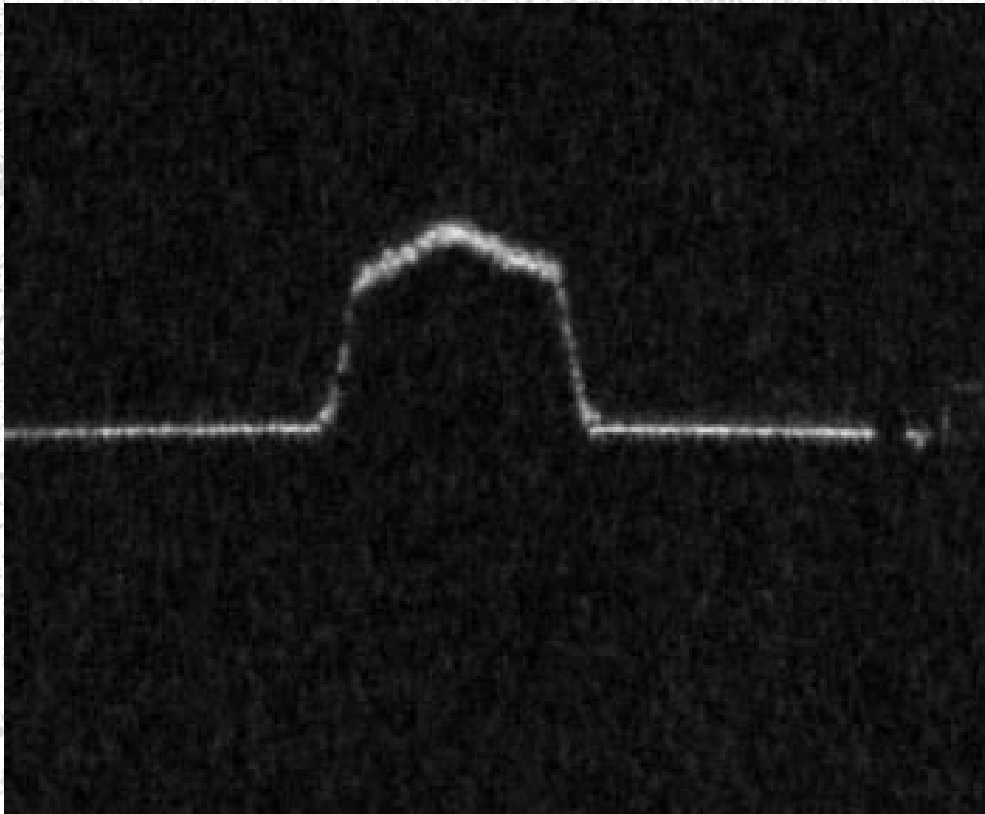
Vibration

Mobile support

after vibration  
at 40Hz during 1min

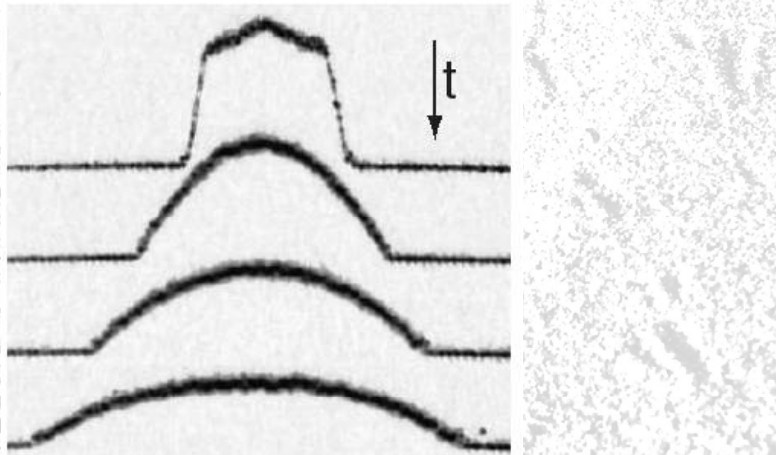
$$h_0 = 3-6 \text{ mm} \ll W_0 = 2-5 \text{ cm}$$

$$f = 26 \text{ Hz}$$

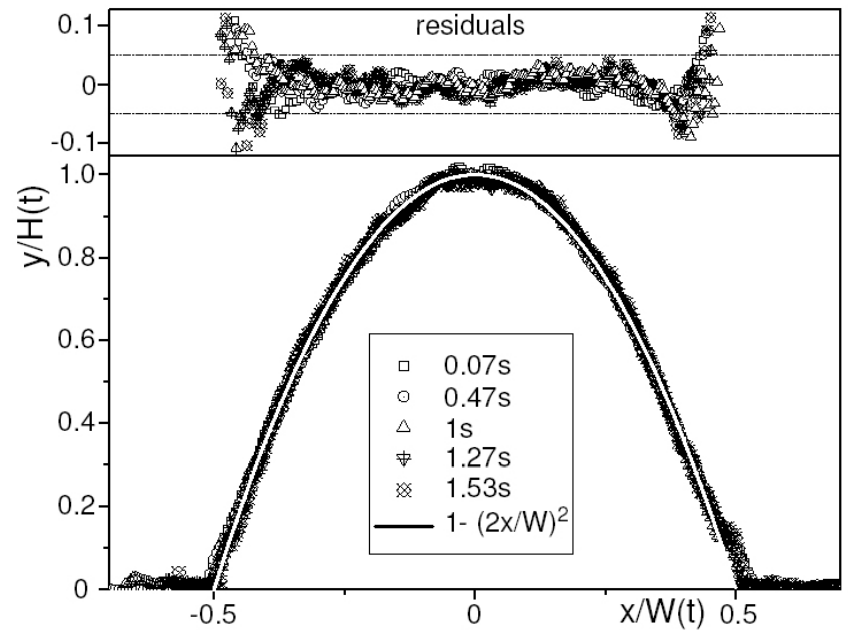


X10

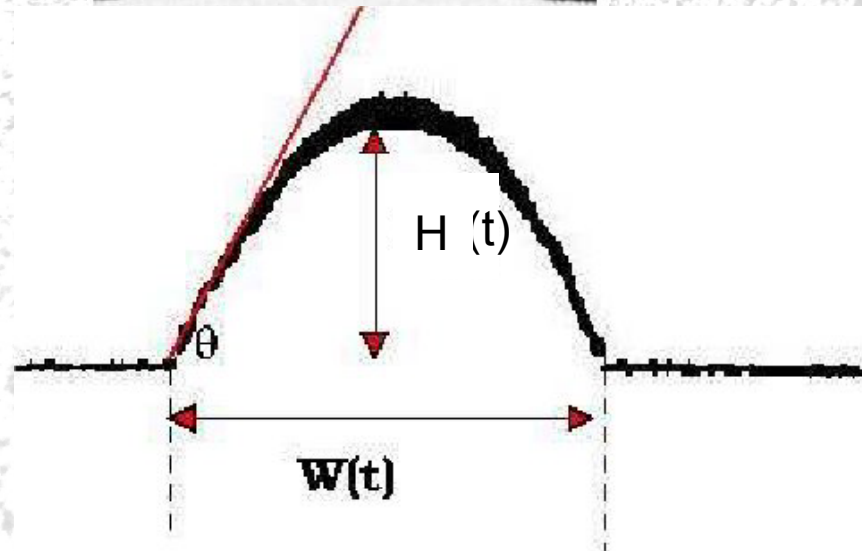
# Universal parabolic profile shape

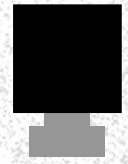


The droplet !

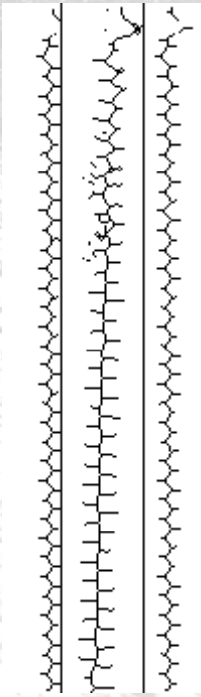
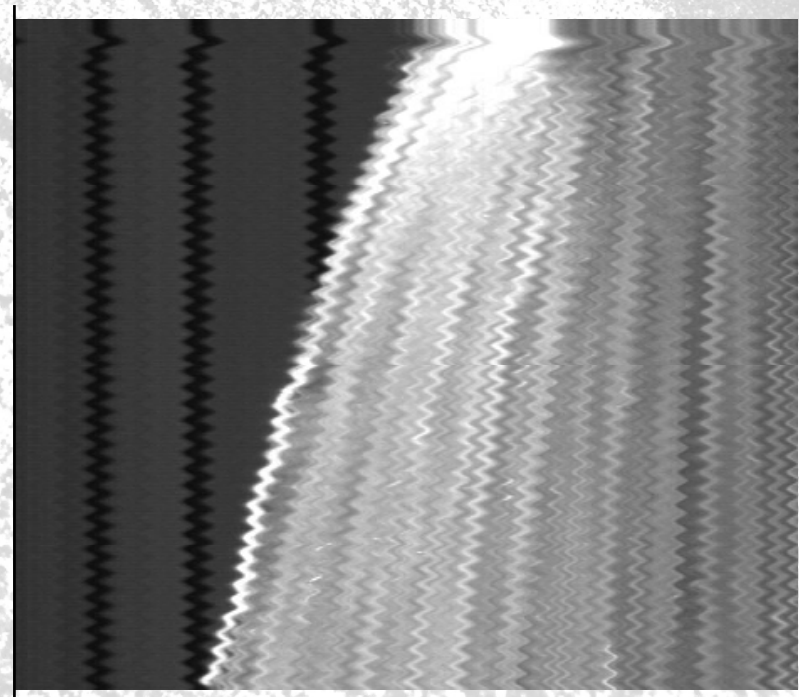
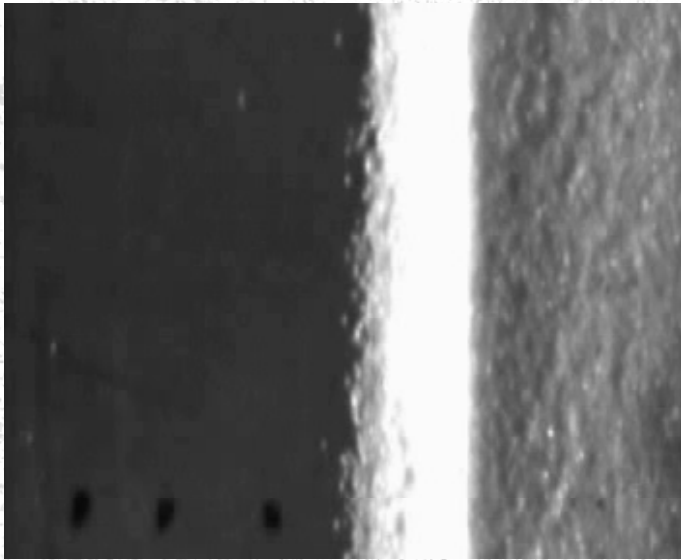


Parabolic profile

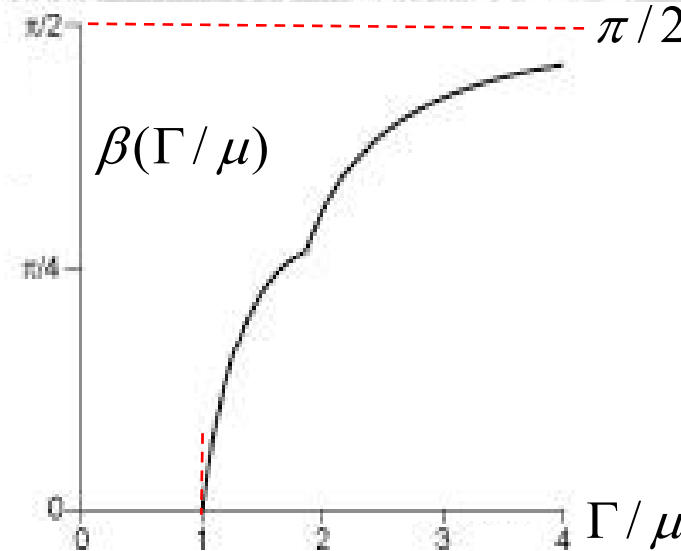
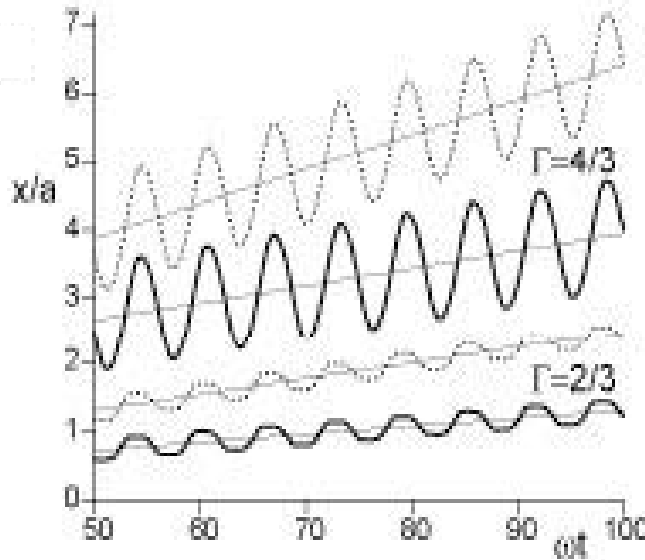
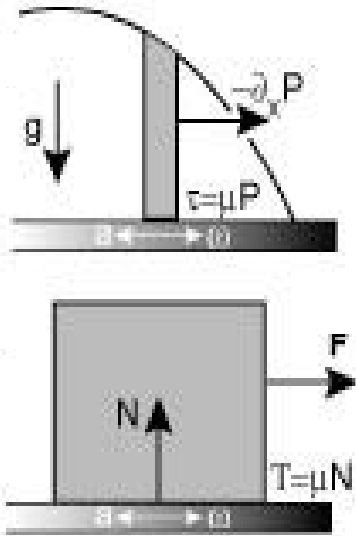




High Speed Camera  
500 im./s



# Sliding Block Model



## Model parameters

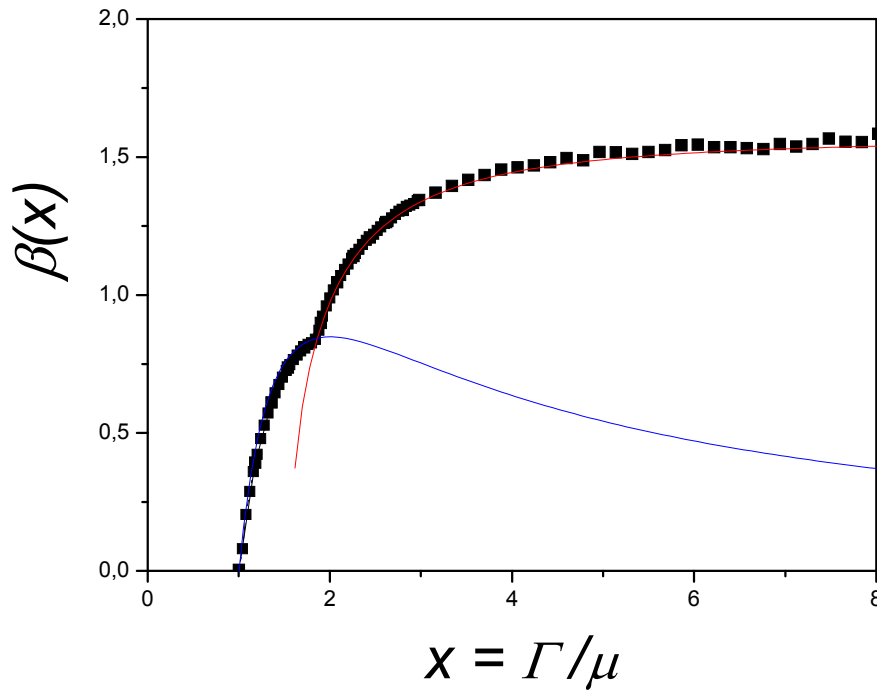
- Harmonic plate motion :  $y_p = a \sin \omega t$
- Sliding friction :  $\mu$
- Relative acceleration :  $\Gamma = a \omega^2 / g$

## Exact result

- Block sliding velocity :  $V = \frac{\beta(\Gamma / \mu)}{\mu} a \omega \frac{F}{N}$



$$F = \frac{\mu}{\beta(\Gamma / \mu)} \frac{V}{a\omega} N$$



Continuous sliding

$$\beta\left(\frac{\Gamma}{\mu}\right) = \frac{\pi}{2} \sqrt{1 - \left(\frac{\pi \mu}{2 \Gamma}\right)^2}$$

Stop/go dynamics

$$\beta\left(\frac{\Gamma}{\mu}\right) = \frac{(\phi - \arcsin(\mu/\Gamma)) \mu}{2\pi \Gamma}$$

$$\cos \phi - \sqrt{1 - (\mu/\Gamma)^2} + \mu/\Gamma(\phi - \arcsin(\mu/\Gamma)) = 0$$

$$J = hV$$

Flux of matter

$$\partial_t h + \partial_x J = 0$$

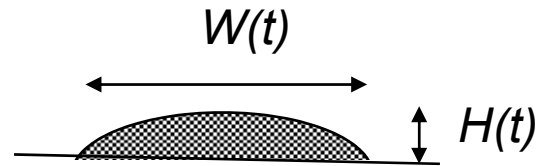
Mass conservation

$$\partial_t h = \partial_x U \partial_x h^2$$

Non-linear diffusion equation

$$\text{with } U = \frac{a\omega}{2\mu} \beta\left(\frac{\Gamma}{\mu}\right)$$

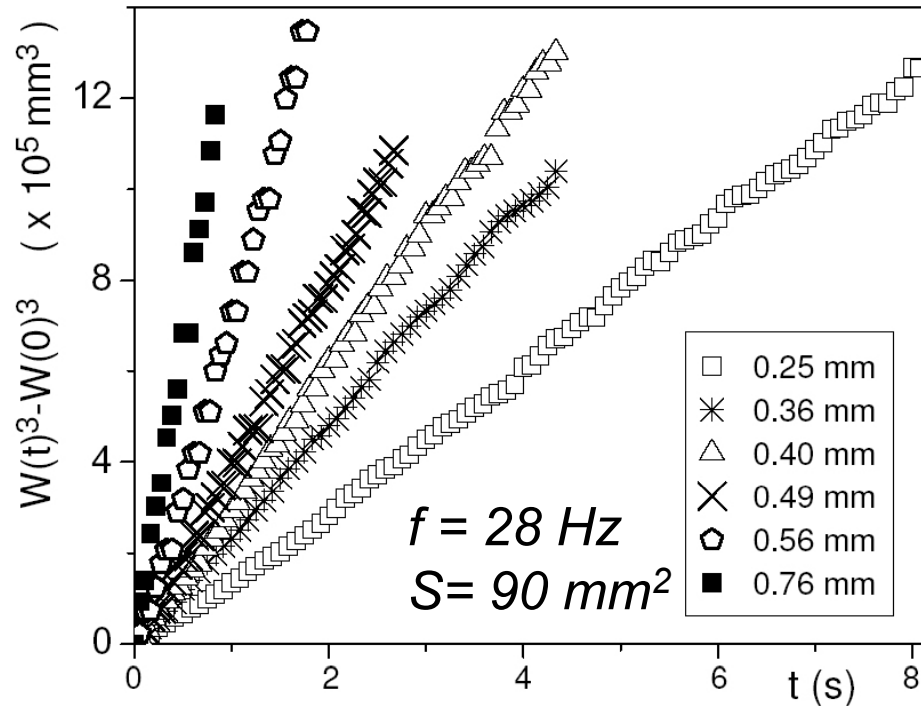
$$S = 2W(t)H(t)/3$$



$$\left\{ \begin{array}{l} h(x,t) = \frac{3S}{2W(t)} \left[ 1 - \left( \frac{2x}{W(t)} \right)^2 \right] \quad \text{Parabolic profile} \\ W^3(t) - W_0^3 \cong \frac{36\pi S a\omega}{\mu} \beta\left(\frac{\Gamma}{\mu}\right) t \quad \text{Spreading law} \end{array} \right.$$

$$\alpha = \frac{36\pi S a\omega}{\mu} \beta\left(\frac{\Gamma}{\mu}\right)$$

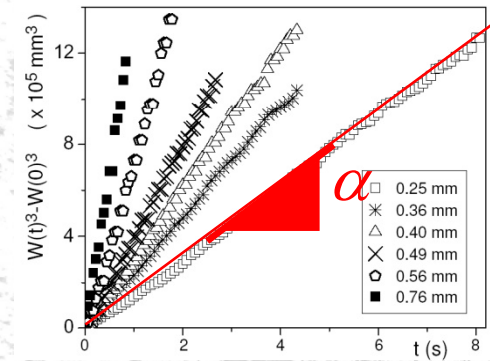
# Spreading dynamics



Experimentally

$$W^3(t) - W_0^3 = \alpha t$$

# An inertial tribometer !



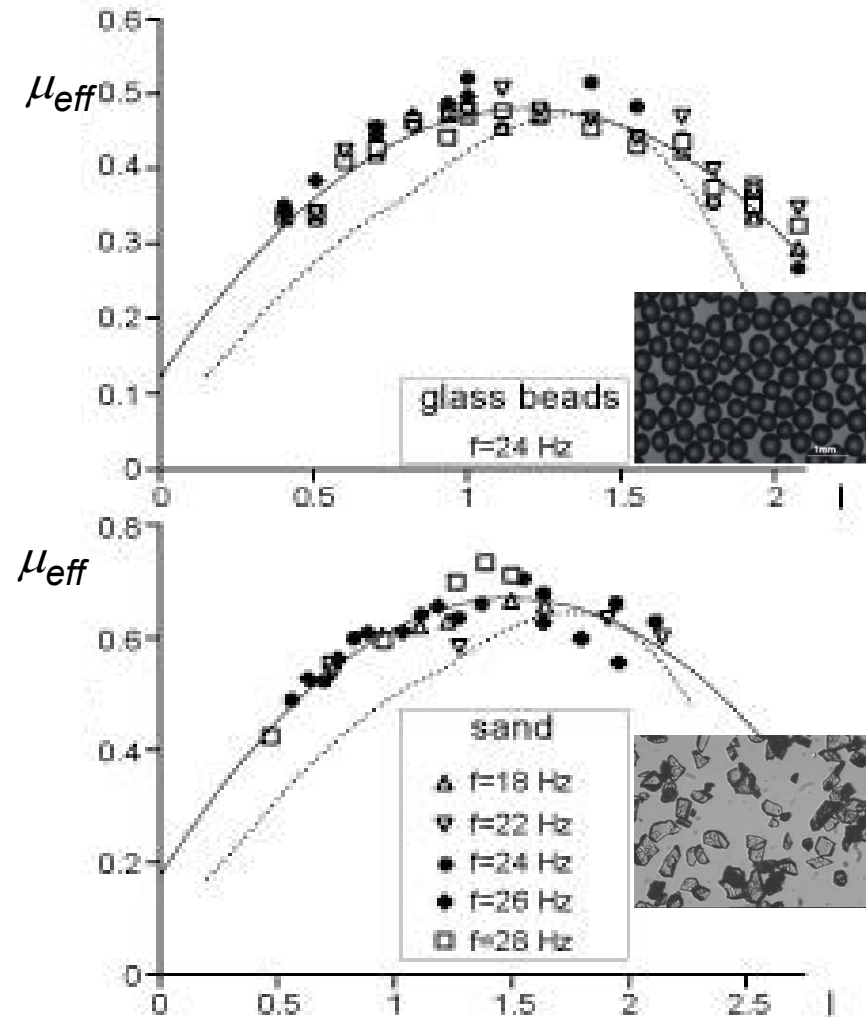
$$\alpha = \frac{dW^3}{dt} = \frac{18gS}{\pi f} \frac{\Gamma}{\mu} \beta\left(\frac{\Gamma}{\mu}\right)$$

Invert the relation

$$\frac{\Gamma}{\mu} \beta\left(\frac{\Gamma}{\mu}\right) = \frac{18gS}{\alpha \pi f}$$

- Get the effective basal friction :  $\mu_{eff}$

# Effective basal friction under vibration

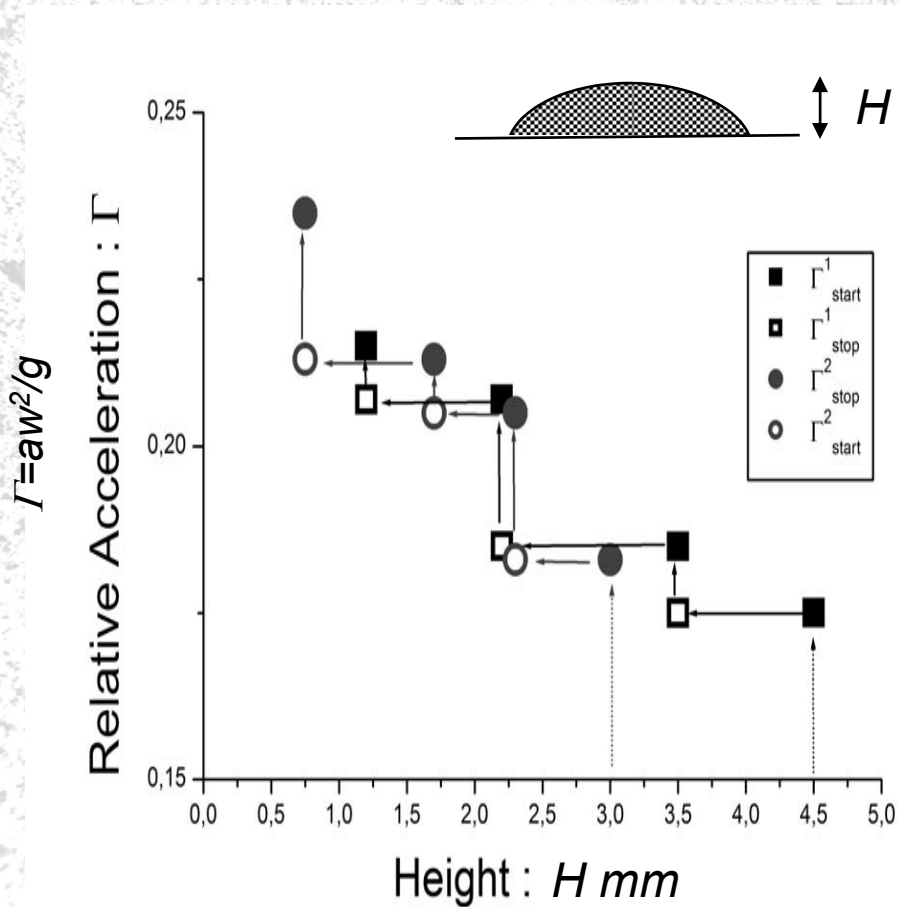


- Measure the effective sliding friction under vibration

$$\mu_{eff}(I) \quad \text{with} \quad I = \frac{a\omega}{\sqrt{gd}}$$

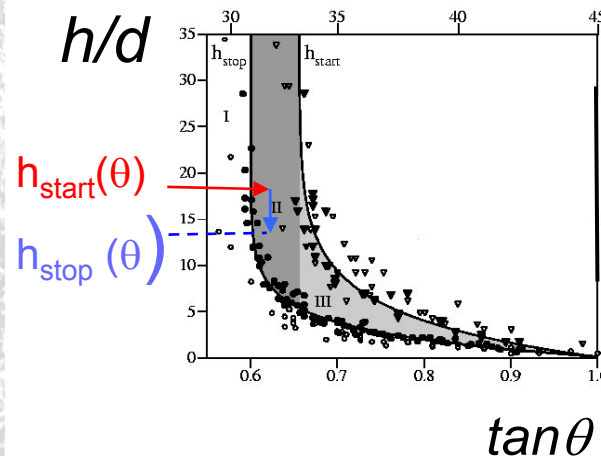
- Hardening (low  $I$ ) and weakening (high  $I$ )

# Dynamics in the metastable domain?



$\mu_s(H)$  and  $\mu_d(H)$  !

Granular layer on a slope



# Conclusions

- A granular film spreads when shaken horizontally



- Parabolic universal shape :

- Spreading law :

$$W^3(t) - W_0^3 = \alpha t$$

- From theory one obtains the effective basal friction :

$$\mu_{eff} (a\omega / (gd))^{1/2}$$

Non monotonous variation !

- Hardening at low vibration

- Weakening at higher vibration